

Using SCALE for Radiation Transport Simulations to Determine Radiation Environment in I²S-LWR

Georgia Tech

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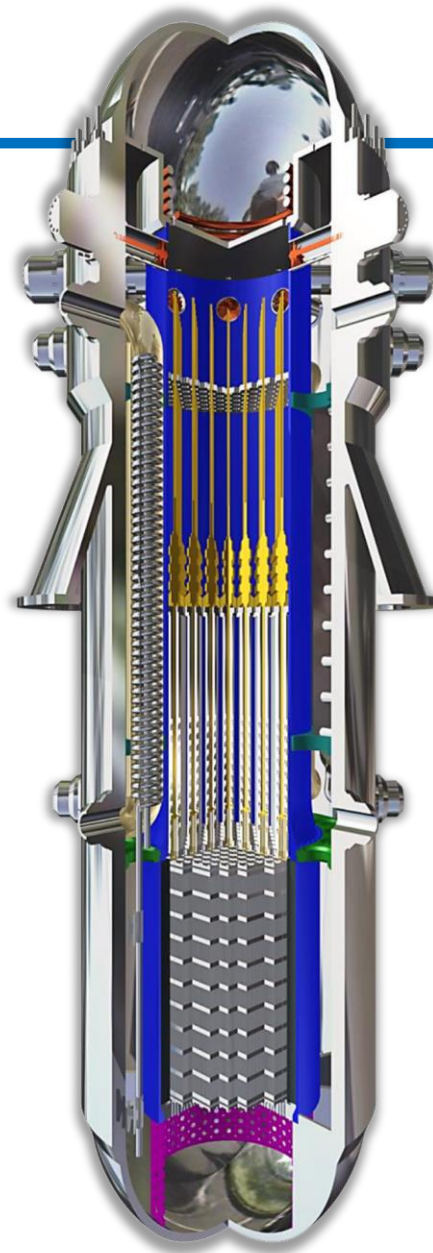
I²S-LWR Background

REQUIREMENTS:

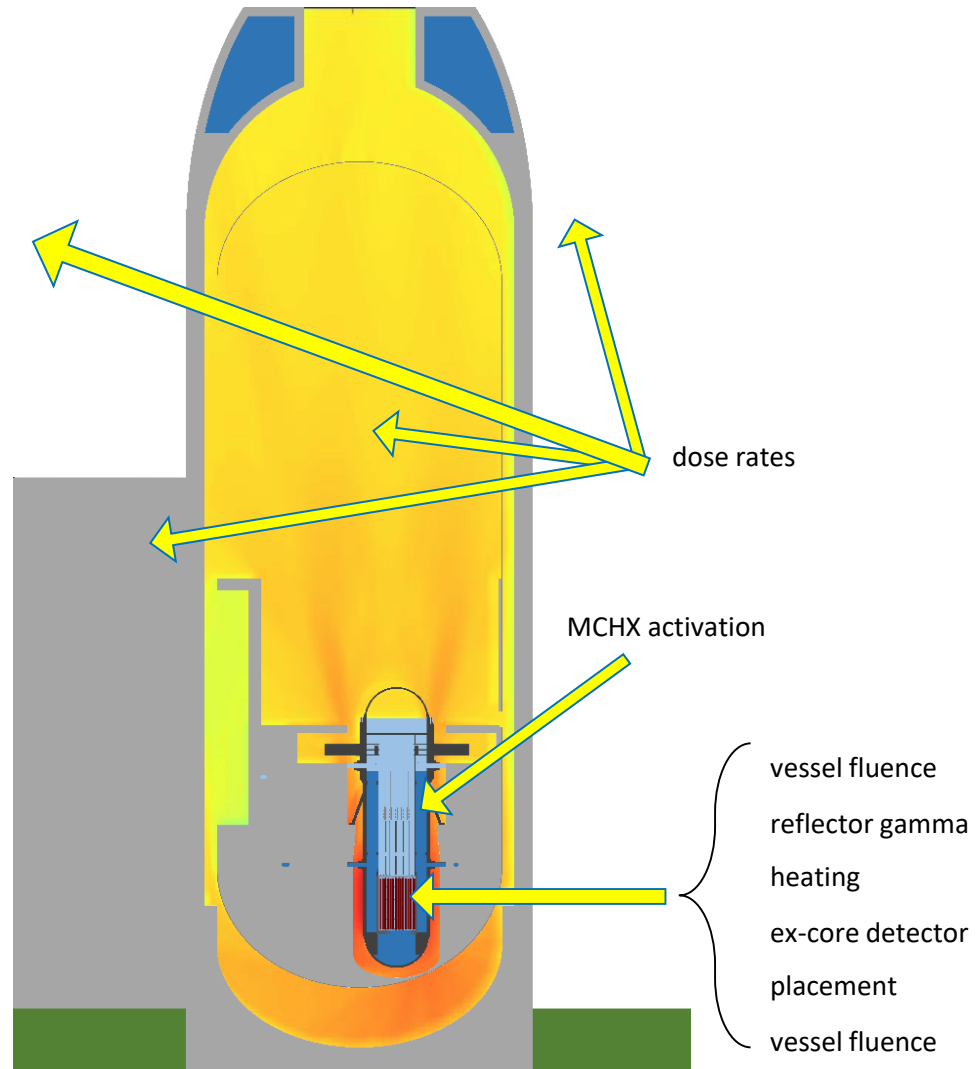
- Large power LWR (1 GWe class) for 'mainstream' US deployment
- Enhanced safety
- Fuel - enhanced accident tolerance
- Economically competitive

KEY TECHNOLOGIES:

- Integral layout
- Integral primary components
- High power density fuel/clad system (silicide fuel / SS cladding)
- High power density (micro-channel type) primary HX (mC-PHX)
- Steam Generation System (mC-PXH + Flashing Drum)

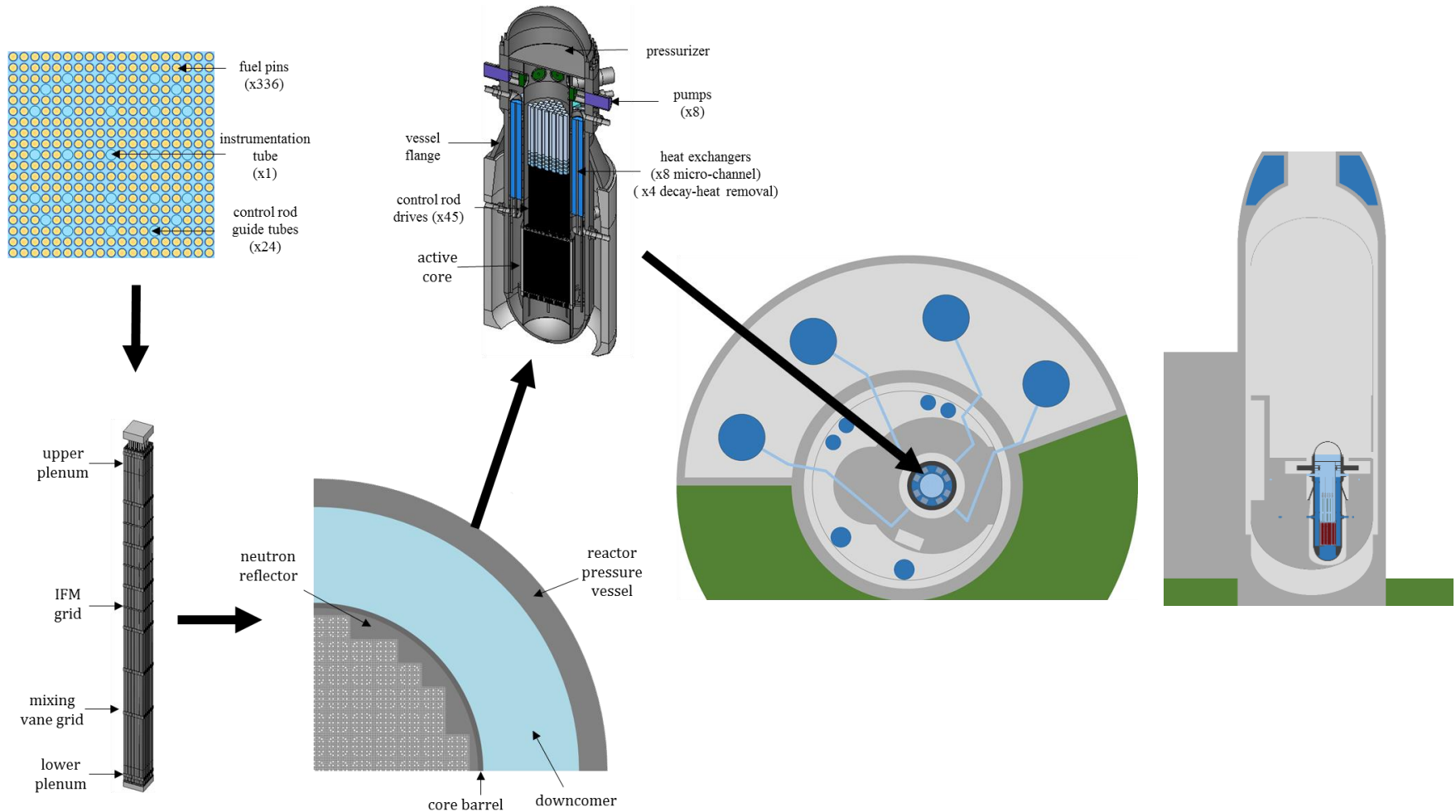


- RPV lifetime assessment
- SiC detector Placement
- Gamma heating in radial neutron steel reflector
- MCHX activation
- Dose in nuclear island



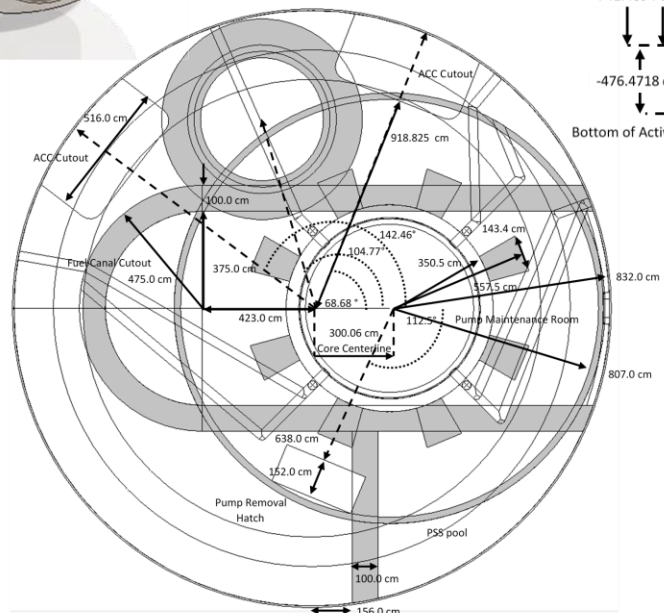
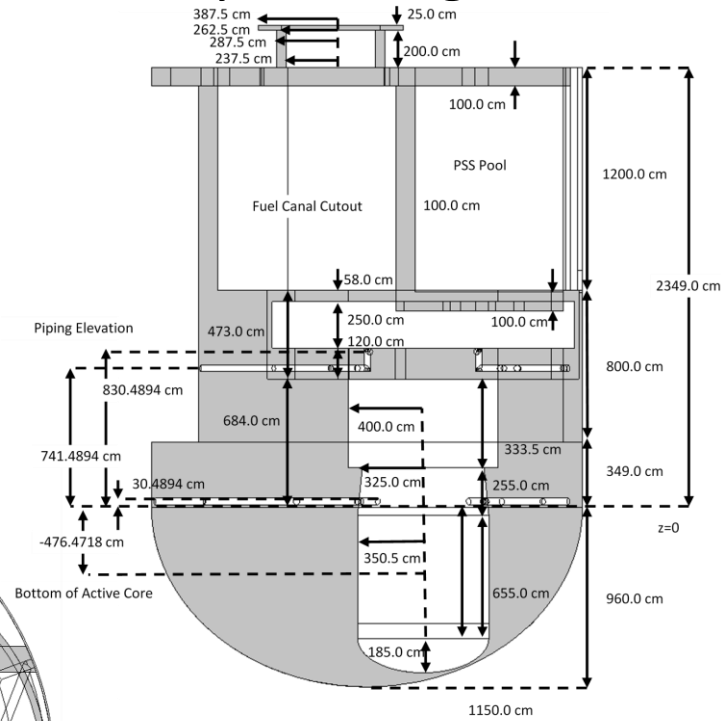
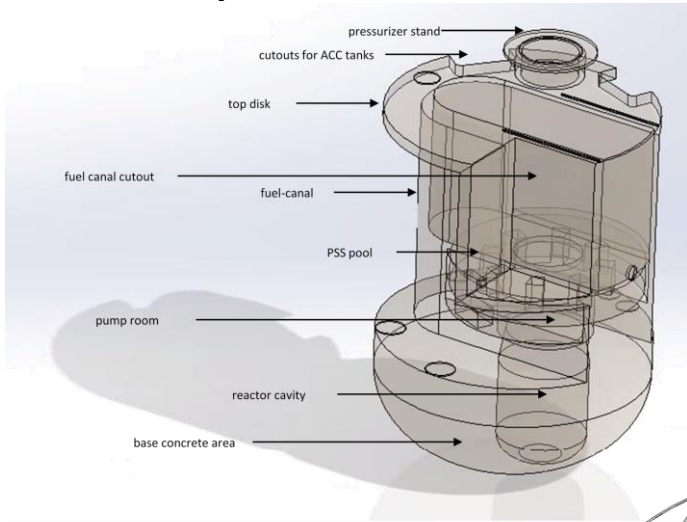
I²S-LWR Shielding Model

- ~ 3000 lines to describe detailed geometry and materials



Containment Vessel Layout

- CV layout extracted from CAD files provided by Westinghouse

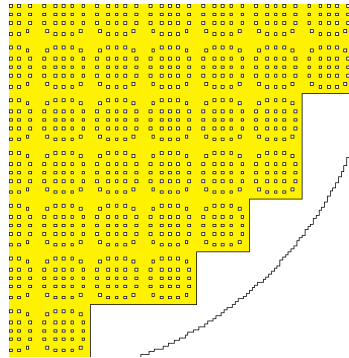




FIXED-SOURCE DESCRIPTIONS

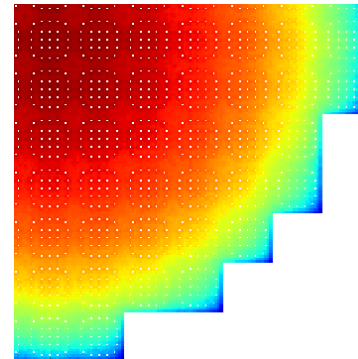
Initial Fixed-Sources

- Preliminary studies using two fixed-source descriptions:
 1. Flat-source: HIGH leakage - conservative for shielding results



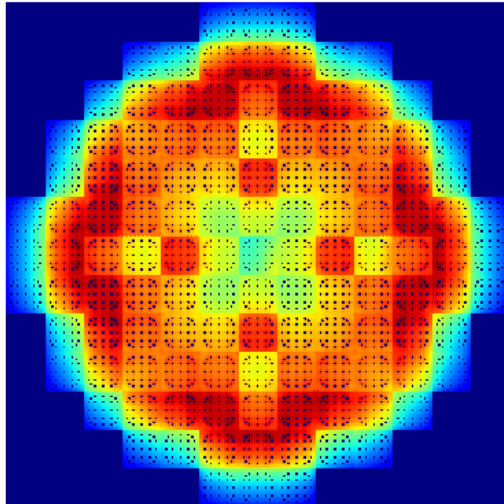
2. Center-peaked Source (fresh fuel / roughly cosine) – LOW leakage – minimum leakage (not conservative)

	7	8	9	10	11	12	13
7	1.955	1.890	1.718	1.445	1.103	0.724	0.355
8	1.900	1.840	1.666	1.398	1.057	0.678	0.308
9	1.727	1.667	1.502	1.242	0.913	0.541	
10	1.447	1.399	1.242	1.000	0.696	0.364	
11	1.102	1.059	0.913	0.695	0.419		
12	0.727	0.680	0.543	0.365			
13	0.359	0.309					



Accurate Fixed-Source description

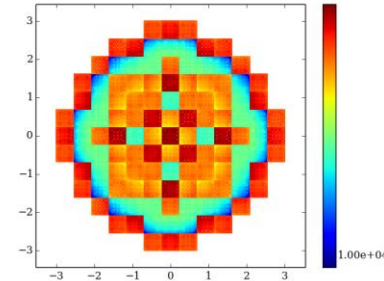
- based on equilibrium cycle from Westinghouse
 - received output file with quarter-core axial pin-wise burnups
 - 225,129 lines



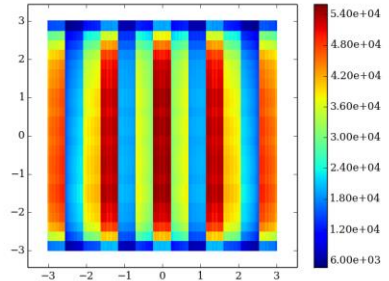
```
sub_mesh_file.py | cargo | readme | cargo.py | u3si2_pinbuoc_half.out
1 ***
2 *** Output File Name: 01_i2s1_eoc_pinburnup_0858.out
3 ***
4
5
6 Assembly ID: H05
7 Assembly Coordinates: 01, 06
8 Assembly Location: 001
9 Channel Quadrant: NE
10 Node Coordinates: 01, 12, 01
11
12 1 2 3 4 5 6 7 8 9 10
13
14
15 1 15335 15219 15180 15213 15272 15150 14997 14823 14723 14767
16
17 2 15933 15349 15167 15291 15760 15280 15032 14757 14598 14673
18
19 3 0 15926 15362 15849 0 16034 15785 15039 14687 14703
20
21 4 16288 15570 15334 15500 16154 16210 0 15708 14887 14803
22
23 5 16331 15600 15353 15504 16113 15810 16135 15882 15062 14884
24
25 6 0 16006 15413 15887 0 16047 16013 0 15475 14944
26
27 7 16146 15480 15251 15353 15832 15386 15310 15581 14959 14836
28
29 8 15591 15323 15195 15211 15320 15197 15108 15062 14801 14768
30
31 9 16061 15486 15302 15420 15893 15425 15326 15605 14967 14792
32
33 10 0 16069 15578 16095 0 16165 16053 0 15560 14921
34
35
36 Maximum Max Minimum Min
37 ===== === ===== ===
38 16331 5-1 14598 2-9
39
40
41 Assembly ID: H05
42 Assembly Coordinates: 01, 06
43 Assembly Location: 001
44 Channel Quadrant: NE
45 Node Coordinates: 01, 12, 02
46
47 1 2 3 4 5 6 7 8 9 10
48
49
50 1 30754 30578 30507 30563 30675 30419 30120 29784 29605 29711
51
52 2 31971 30881 30571 30900 31971 30913 30380 29788 29424 29514
53
54 3 0 32126 31010 32213 0 32675 32149 30479 29639 29544
55
56 4 32544 31308 30969 31442 32938 33090 0 31980 30067 29717
57
58 5 32583 31347 31001 31448 32844 32200 32926 32342 30445 29863
59
60 6 0 32236 31099 32299 0 32699 32632 0 31348 29984
61
62 7 32235 31075 30735 31061 32178 31191 31029 31626 30184 29764
63
64 8 31036 30707 30556 30643 30890 30657 30473 30351 29779 29629
65
66 9 32136 31002 30645 30922 31959 30944 30754 31397 30037 29655
67
68 10 0 32110 30948 32055 0 32148 31963 0 31094 29829
69
```


Fixed-Source description

- developed python script with detailed classes to define full-core
- read in data from text file and look at burnups (MWd/MTHM)
- Need to convert to average fission power distribution
- Known: final BU, shuffling pattern
- Assume: ΔBU is average power
- Create map of full-core shuffling pattern
- Extend python classes to read in assembly shuffling pattern and positioning
- $\Delta BU_{\text{cycle}} = \Delta BU_{\text{final}} - \Sigma \Delta BU_{\text{previous}}$



radial BU with linear scale

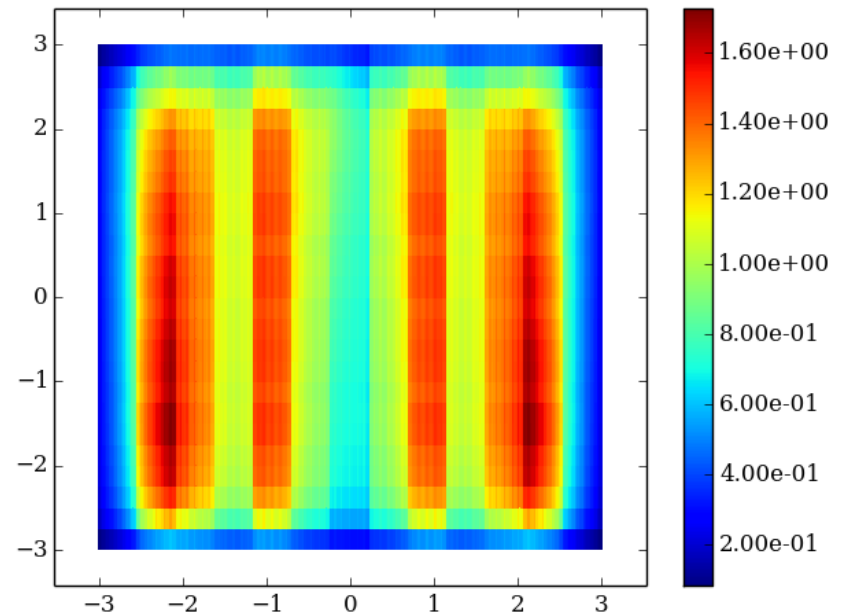
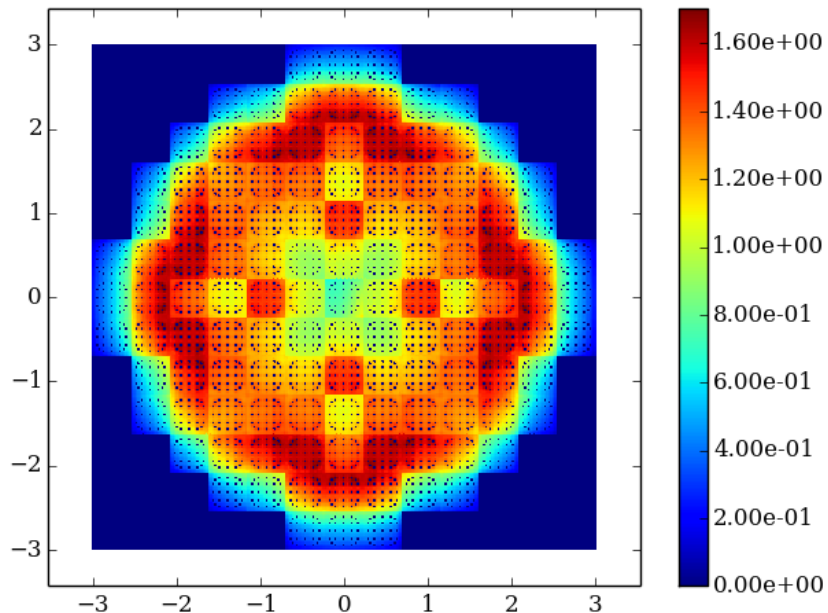


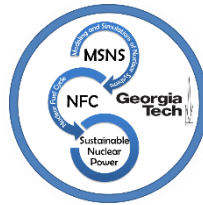
axial burnup with log scale

	N	M	L	K	J	H	G	F	E	D	C	B	A		N	M	L	K	J	H	G	F	E	D	C	B	A		
1	N1	M1	L1	K1	J1	H1	G1	F1	E1	D1	C1	B1	A1	1	1	00	00	00	00	00	J4	G11	E4	00	00	00	00	1	
2	N2	M2	L2	K2	J2	H2	G2	F2	E2	D2	C2	B2	A2	2	2	00	00	00	H4	J8	FR	FR	FR	FR	F8	F4	00	00	2
3	N3	M3	L3	K3	J3	H3	G3	F3	E3	D3	C3	B3	A3	3	3	00	00	G6	FR	FR	FR	G2	FR	FR	FR	F7	00	00	3
4	N4	M4	L4	K4	J4	H4	G4	F4	E4	D4	C4	B4	A4	4	4	00	K6	FR	G9	D11	B8	E5	M8	K11	J7	FR	D6	00	4
5	N5	M5	L5	K5	J5	H5	G5	F5	E5	D5	C5	B5	A5	5	5	00	F5	FR	C10	J3	L8	FR	L6	C5	L10	FR	H5	00	5
6	N6	M6	L6	K6	J6	H6	G6	F6	E6	D6	C6	B6	A6	6	6	K5	FR	FR	F12	H11	K4	J11	D4	H3	H12	FR	FR	D5	6
7	N7	M7	L7	K7	J7	H7	G7	F7	E7	D7	C7	B7	A7	7	7	C7	FR	M7	J5	FR	C9	K2	L5	FR	E9	B7	FR	L7	7
8	N8	M8	L8	K8	J8	H8	G8	F8	E8	D8	C8	B8	A8	8	8	K9	FR	FR	F2	F11	K10	E3	D10	F3	H2	FR	FR	D9	8
9	N9	M9	L9	K9	J9	H9	G9	F9	E9	D9	C9	B9	A9	9	9	00	F9	FR	C4	L9	C8	FR	C6	E11	L4	FR	H9	00	9
10	N10	M10	L10	K10	J10	H10	G10	F10	E10	D10	C10	B10	A10	10	10	00	K8	FR	E7	D3	B6	J9	M6	K3	G5	FR	D8	00	10
11	N11	M11	L11	K11	J11	H11	G11	F11	E11	D11	C11	B11	A11	11	11	00	00	H7	FR	FR	FR	G12	FR	FR	FR	G8	00	00	11
12	N12	M12	L12	K12	J12	H12	G12	F12	E12	D12	C12	B12	A12	12	12	00	00	00	H10	J6	FR	FR	FR	E6	F10	00	00	00	12
13	N13	M13	L13	K13	J13	H13	G13	F13	E13	D13	C13	B13	A13	13	13	00	00	00	00	00	J10	G3	E10	00	00	00	00	00	13
	N	M	L	K	J	H	G	F	E	D	C	B	A		N	M	L	K	J	H	G	F	E	D	C	B	A		

Fixed-Source description

- total peaking factor of 1.69 (very close to expected value of 1.7)
- (assumed watt fission spectrum for uranium everywhere ... plutonium has a harder spectrum and therefore more leakage)

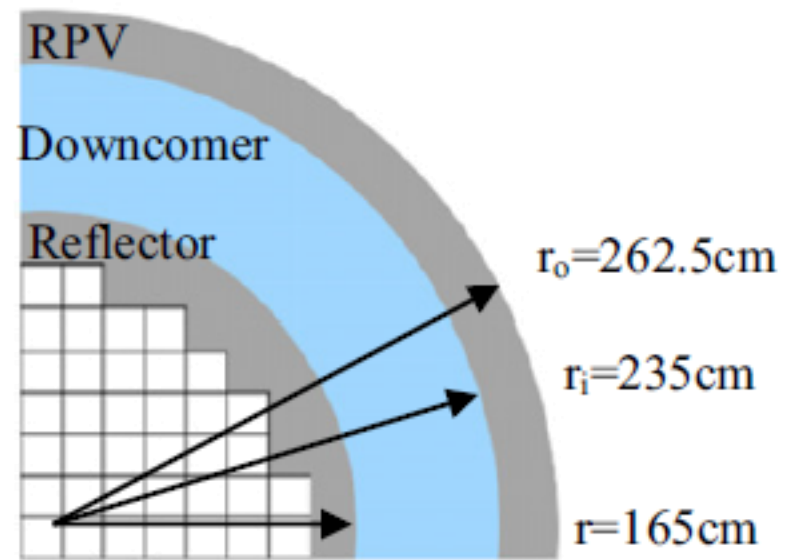




REACTOR PRESSURE VESSEL LIFETIME ASSESSMENT

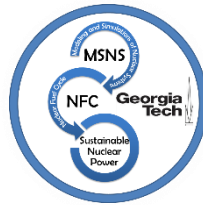
RPV lifetime assessment

- Will the reactor vessel rupture in a 100 year lifetime?
- Fast neutron fluence (>1MeV) in steels
 - slowly degrades mechanical properties through neutron embrittlement based on Cu and Ni in steel and welds
 - lifetime fluence cutoff $2e19 \text{ n/cm}^2$
- based on preliminary design
- 2 fixed-source neutron sources
 - high-leakage, flat source
 - low-leakage, center-peaked source
- 3 ratios of volume percent of steel/water in reflector
 - 100/0
 - 90/10
 - 70/30



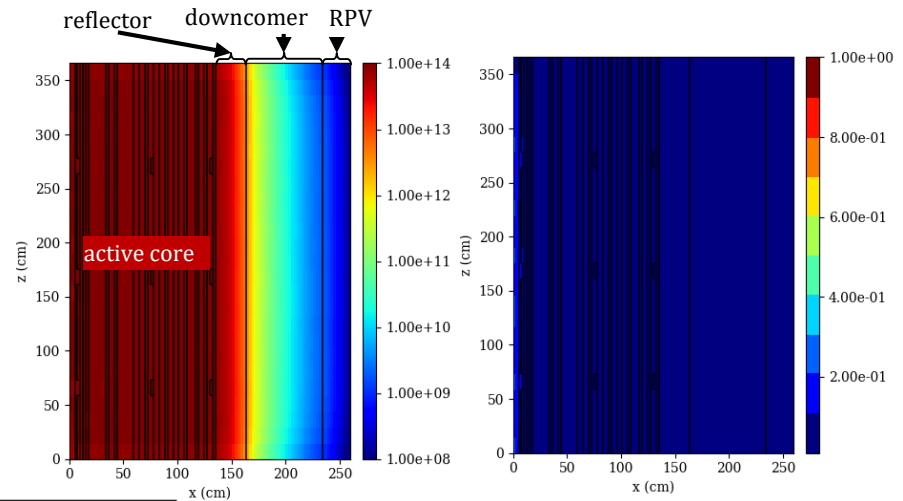
radial view of RPV layout

RPV lifetime assessment

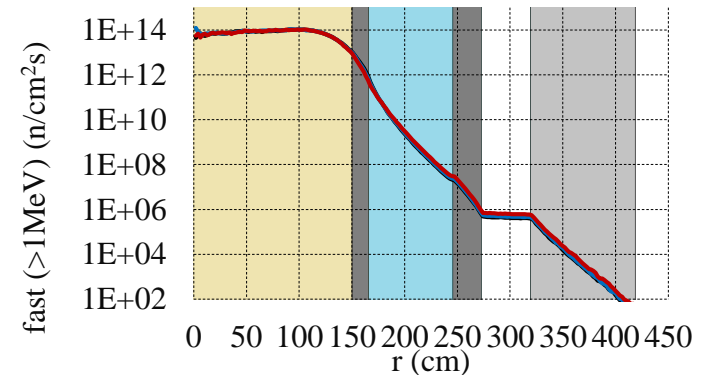


- “Radiation Damage Assessment in the Reactor Pressure Vessel of the Integral Inherently Safe Light Water Reactor (I2S-LWR)”, ISRD-15, published 2016 EPJ Web of Conferences

high leakage core w/
steel/water ratio 70/30 in
reflector is safe for 100 year
lifetime



Case	100-year Fast Fluence ($> 1 \text{ MeV}$) [$(10^{19}) \text{ n/cm}^2$]					DPA/s	100-year DPA
	Max**	Avg. 1/8T	Avg. 1/4T	Avg. 1/2T	Avg. 3/4T		
Flat (70/30*)	1.531±1%	0.805±1%	0.584±1%	0.266±1%	0.112±1%	3.14E-12±2%	8.93E-03±4%
Flat (90/10*)	1.148±1%	0.627±1%	0.451±1%	0.204±1%	0.086±1%	2.47E-12±2%	7.01E-03±4%
Flat (100/0*)	1.060±2%	0.552±1%	0.395±2%	0.178±2%	0.075±2%	2.24E-12±4%	6.38E-03±4%
Center-peaked (70/30*)	0.143±2%	0.076±2%	0.052±2%	0.021±2%	0.008±2%	4.08E-13±2%	1.16E-03±2%
Center-peaked (90/10*)	0.118±1%	0.058±2%	0.040±2%	0.017±2%	0.006±2%	3.22E-13±2%	9.14E-04±2%
Center-peaked (100/0*)	0.113±3%	0.054±2%	0.037±2%	0.015±3%	0.006±4%	2.87E-13±2%	8.15E-04±2%



*The numbers represent ratios of homogenized steel-water volume percentages.

**Max and Avg. refer to azimuthal maximum and average values found at an elevation of the core midplane and radially in the inner portion of the RPV.



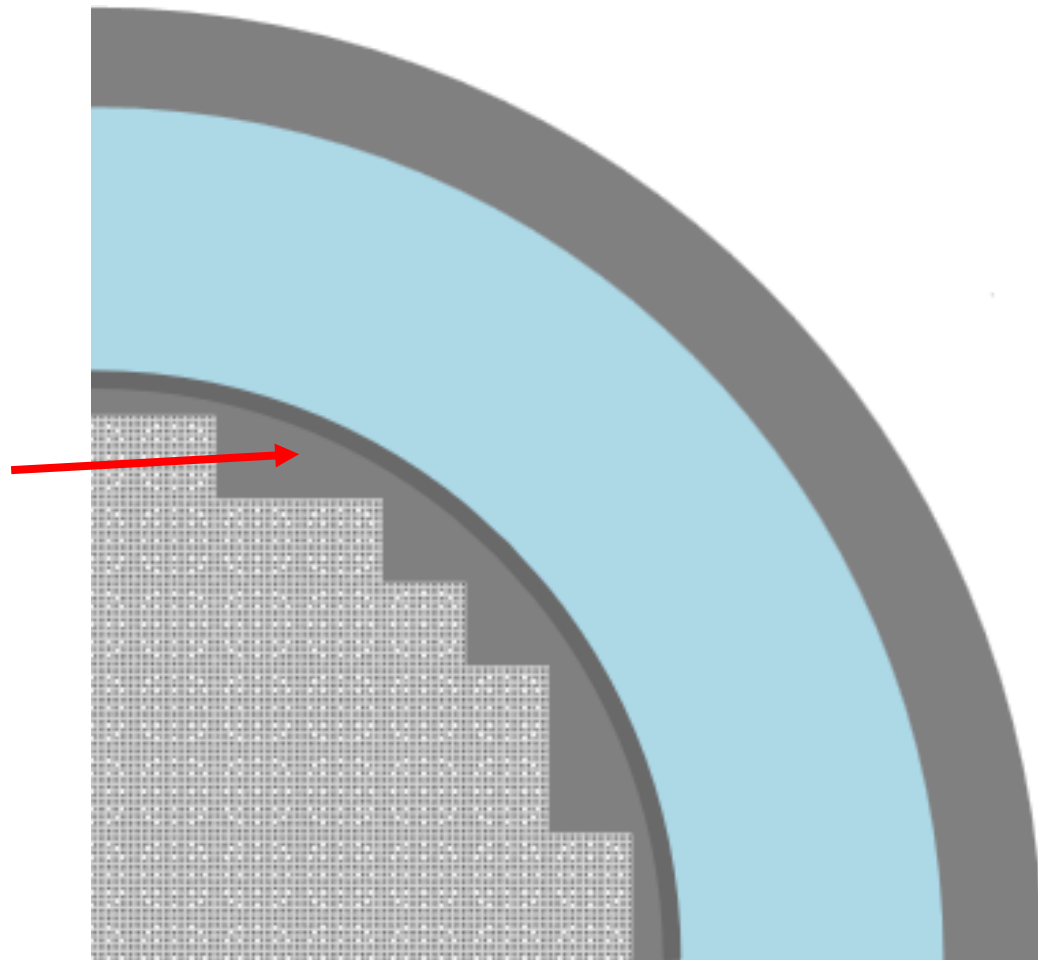
GAMMA HEATING IN RADIAL NEUTRON REFLECTOR

Gamma Heating in Reflector

- KERMA (kinetic energy released per unit mass) factors for $n+\gamma$ heating
 - not a default in MAVRIC
 - extracted from updated BUGLE-96 shielding library (developed @ ORNL)

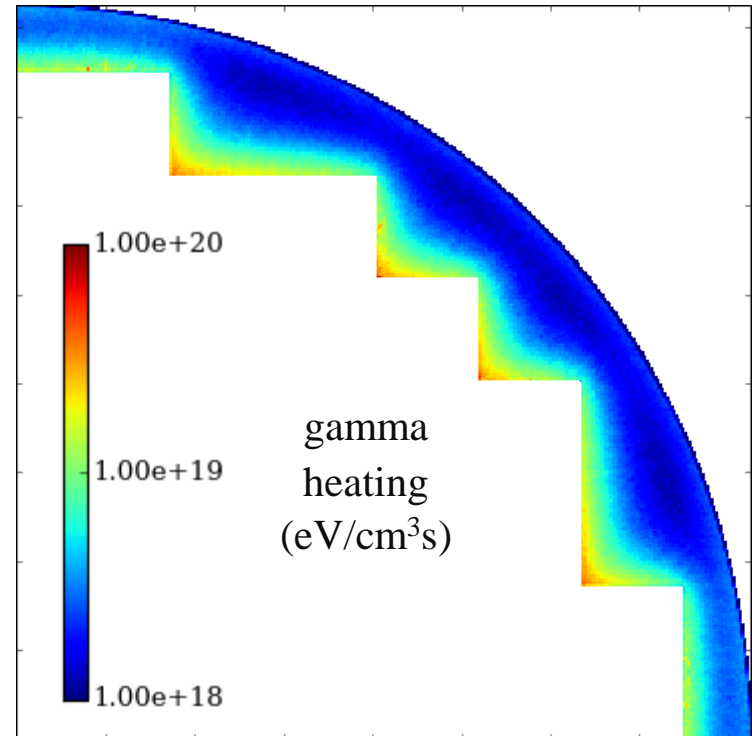
- Adjoint solution
 - Adjoint source: $n+\gamma$ KERMA factors in reflector
 - 27n+19g multigroup library
 - 128x128x106 mesh
 - S_4P_1

- Parallel MC
 - 32 simulations
 - 6 hours of wall time

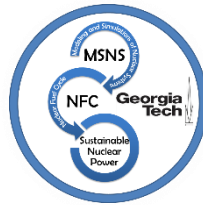


Gamma Heating in Reflector

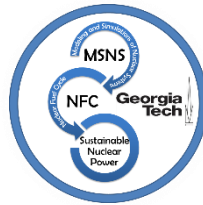
- 5.95 MW generated in reflector
 - large amount of heat
 - about what expected
 - not a problem for cooling channel designs with low water volume



“Calculating Gamma Heating in the I²S-LWR Radial Steel Reflector”, Timothy Flaspoeehler and Bojan Petrovic, ANS Winter Conference.



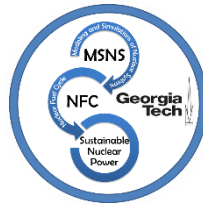
EX-CORE SILICON CARBIDE DETECTOR PLACEMENT



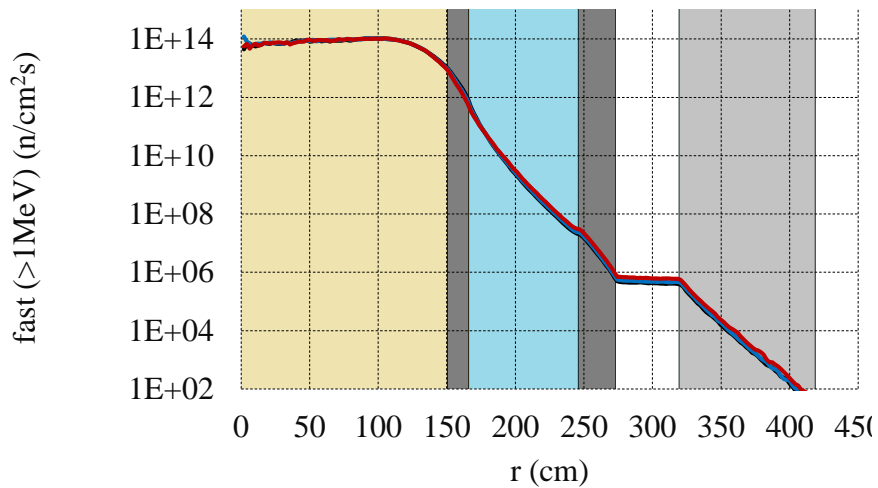
ex-Core SiC Detector Placement

- GOAL: balance radiation damage vs. sensitivity
 - large downcomer region (good as shield, bad for ex-core detectors)
 - SiC can detect fast and thermal neutrons
- 12 separate cases
 - 4 boron concentrations (0,500,1000,1500 ppm)
 - 3 reflector homogenizations (100/0, 90/10, 70/30)
- Adjoint solution
 - adjoint source: entire flux radially through concrete cavity
 - 27 group library
 - P_3/S_8
 - 128x128x64 mesh
 - 30 minutes on 8 CPUs per solution
- MC tallies
 - 12 hour simulations
 - ~ 65 million source particles

ex-Core SiC Detector Placement

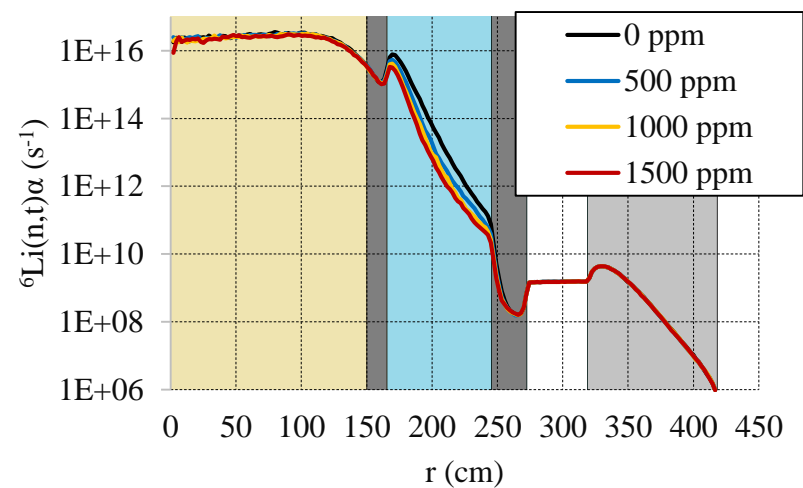


Fast Flux Damage

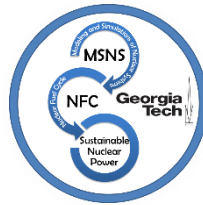


vs

Thermal Flux Response



ex-Core SiC Detector Placement



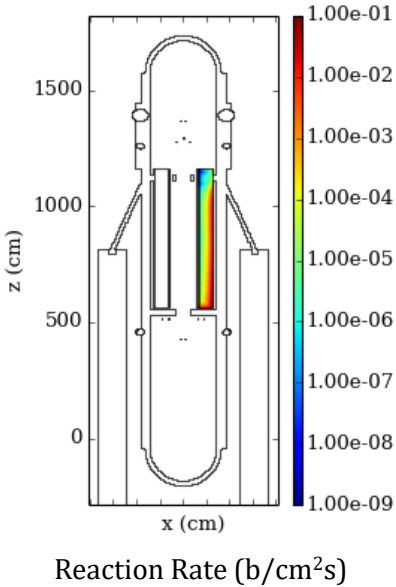
- Results: feasible to have detector with enough resolution that can last the lifetime of the plant without being replaced

radial position (cm)	fast flux E>1MeV (cm ⁻² s ⁻¹)	30 year fast fluence (cm ⁻²)	60 year fast fluence (cm ⁻²)	100 year fast fluence (cm ⁻²)	thermal flux E<0.625eV (cm ⁻² s ⁻¹)				6Li depletion (% per year)	thermal monitor lifetime
					0 ppm	500 ppm	1000 ppm	1500 ppm		
165	8.92E+11	8.45E+20	1.69E+21	2.53E+21	6.19E+12	4.62E+12	3.96E+12	3.51E+12	11.2	move or shield
170	2.89E+11	2.74E+20	5.48E+20	8.22E+20	2.10E+13	1.44E+13	1.11E+13	9.20E+12	40.6	move or shield
175	8.16E+10	7.72E+19	1.54E+20	2.32E+20	1.35E+13	6.99E+12	4.70E+12	3.59E+12	26.3	move or shield
185	2.03E+10	1.92E+19	3.85E+19	5.77E+19	3.15E+12	1.22E+12	6.87E+11	4.19E+11	6.14	replace each cycle
195	4.67E+09	4.42E+18	8.84E+18	1.33E+19	4.66E+11	1.08E+11	5.83E+10	3.39E+10	0.908	may be replaced
205	1.24E+09	1.17E+18	2.34E+18	3.51E+18	5.76E+10	1.53E+10	6.57E+09	4.58E+09	0.112	may be replaced
215	4.18E+08	3.96E+17	7.91E+17	1.19E+18	1.05E+10	2.79E+09	1.83E+09	1.21E+09	0.0203	plant lifetime
225	1.34E+08	1.27E+17	2.54E+17	3.80E+17	2.00E+09	6.70E+08	4.61E+08	3.26E+08	3.85E-03	plant lifetime
235	5.03E+07	4.76E+16	9.53E+16	1.43E+17	6.07E+08	2.33E+08	1.43E+08	1.15E+08	1.18E-03	plant lifetime
245	2.38E+07	2.25E+16	4.50E+16	6.75E+16	1.99E+08	9.54E+07	6.49E+07	4.92E+07	3.82E-04	plant lifetime
cavity	4.34E+05	4.11E+14	8.22E+14	1.23E+15	1.82E+06	1.82E+06	1.83E+06	1.82E+06	4.17E-06	plant lifetime

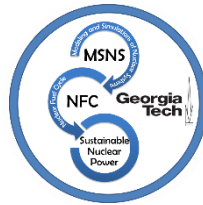
Detector Placement
Good Value
Acceptable but not ideal
High damage or low response

“Feasibility of Ex-Core In-Vessel Nuclear Instrumentation for Integral Inherently Safe Light Water Reactor (I2S-LWR)”, Bojan Petrovic, Timothy Flaspoebler, The 2015 International Conference on Applications of Nuclear Techniques, Crete, Greece, June 14-20, 2015

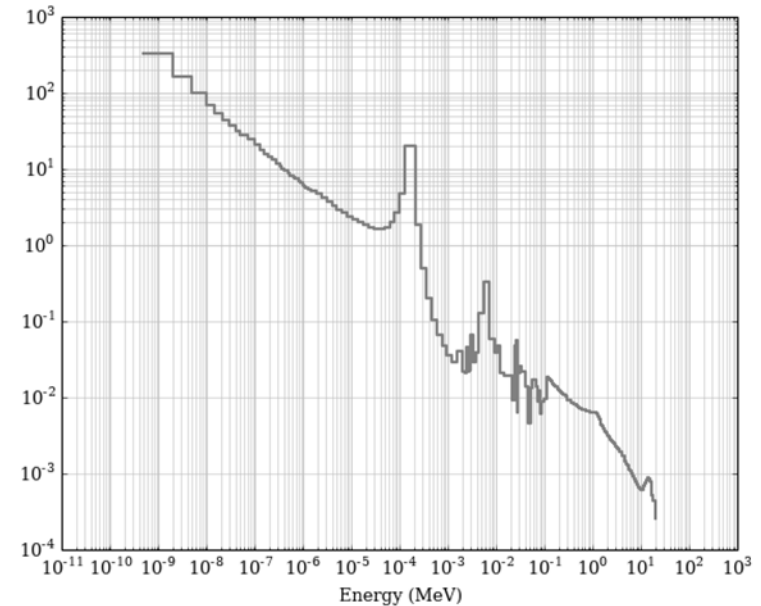
MICRO-CHANNEL HEAT EXCHANGER ACTIVATION



MCHX Activation

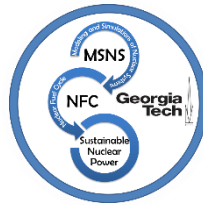


- reference
 - AP1000 DCD (*Design Control Document*) defines impurity levels in primary steel components (close to the core):
 - » maximum 0.05 w/o of Cobalt
- ^{59}Co (100% of natural cobalt) impurities generate ^{60}Co
- ^{60}Co ($t_{1/2}=5.27$ yr) beta decays emitting 1.17 and a 1.33 MeV gamma rays

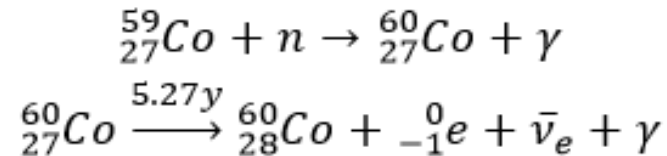


Cross Section for $^{59}\text{Co}(n,\gamma)^{60}\text{Co}$.

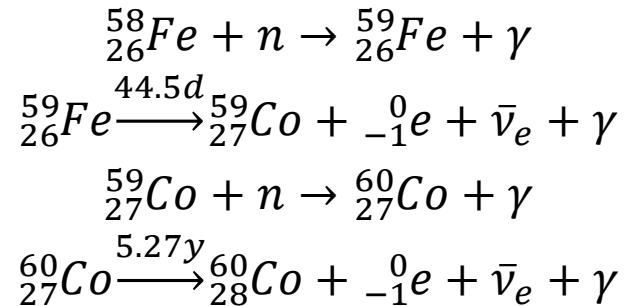
MCHX Activation



- Different Pathways
 - impurities

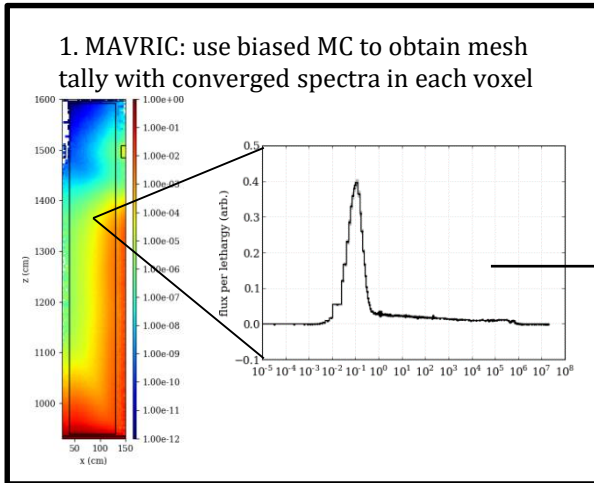


- iron isotopes



- (?) possible unknown pathways

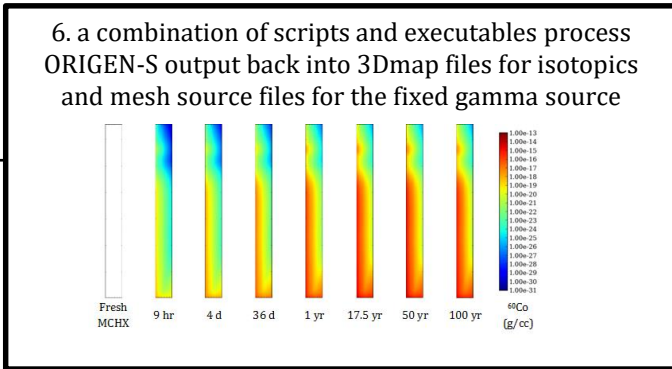
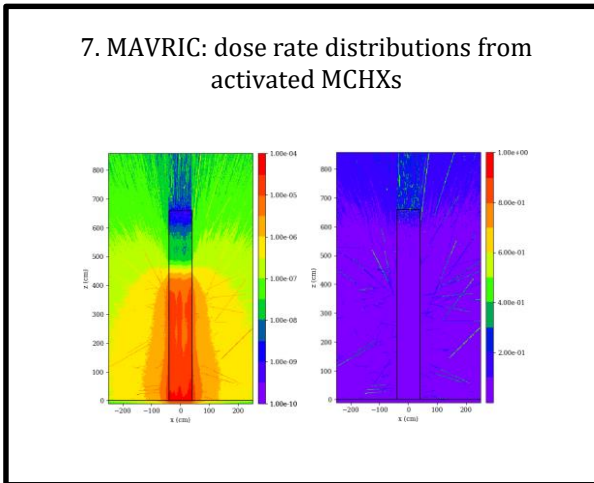
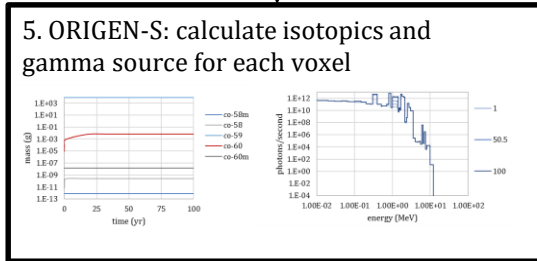
MCHX Activation



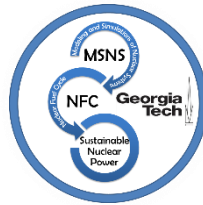
2. CSAS-MG: generate 238-group AMPX master library

3. AJAX: convert AMPX master library to AMPX working library

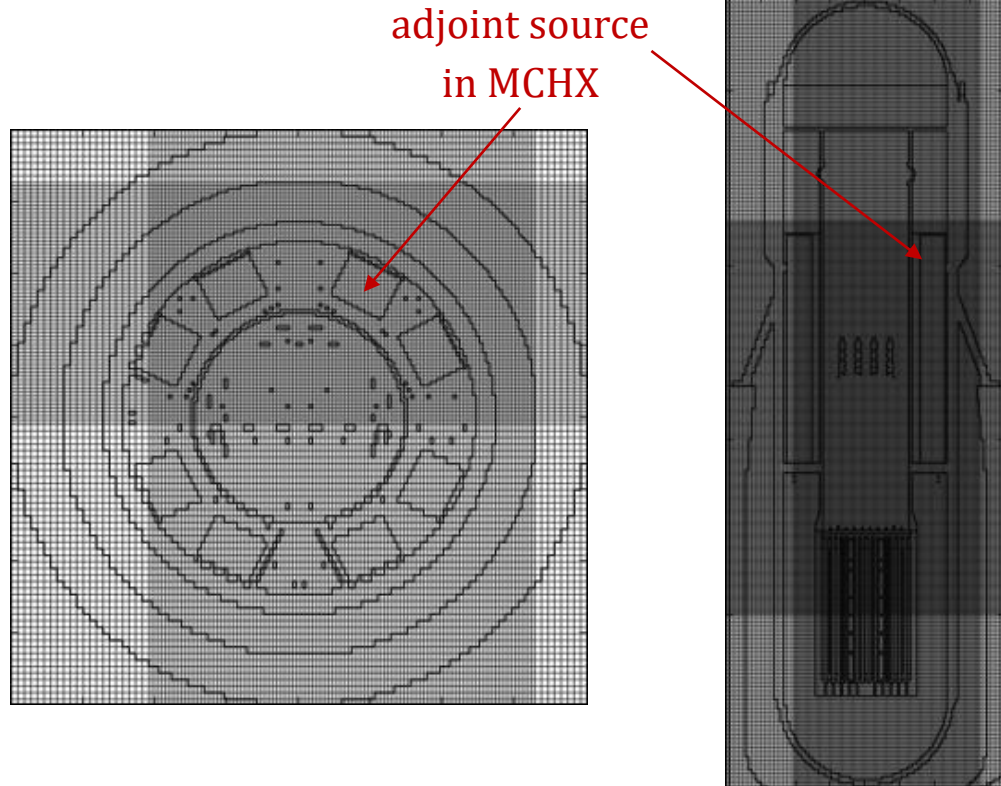
4. COUPLE: collapse 238-group working library to 1-group activation library



MCHX Activation

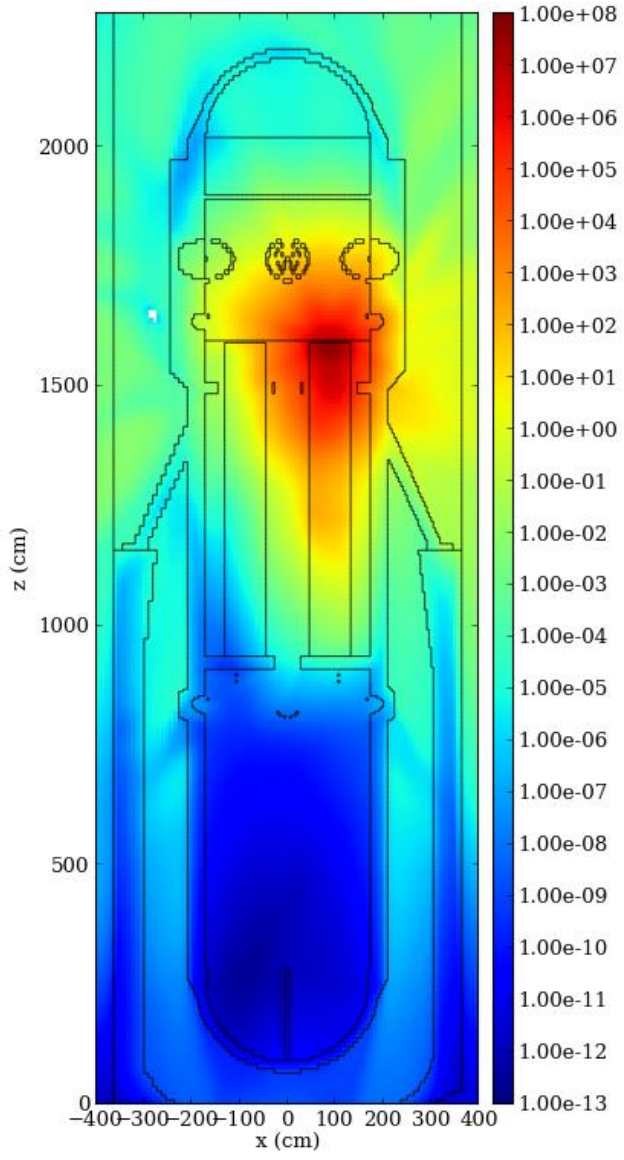


- Adjoint source
 - FW-CADIS
 - total neutron flux in MCHX
- Adjoint solution
 - Coarse-group library provided poor MC results
 - 238-group library refined mesh (147x125x370)
 - P_1S_4 Legendre scattering / quadrature set
 - 12.2 Gb importance map

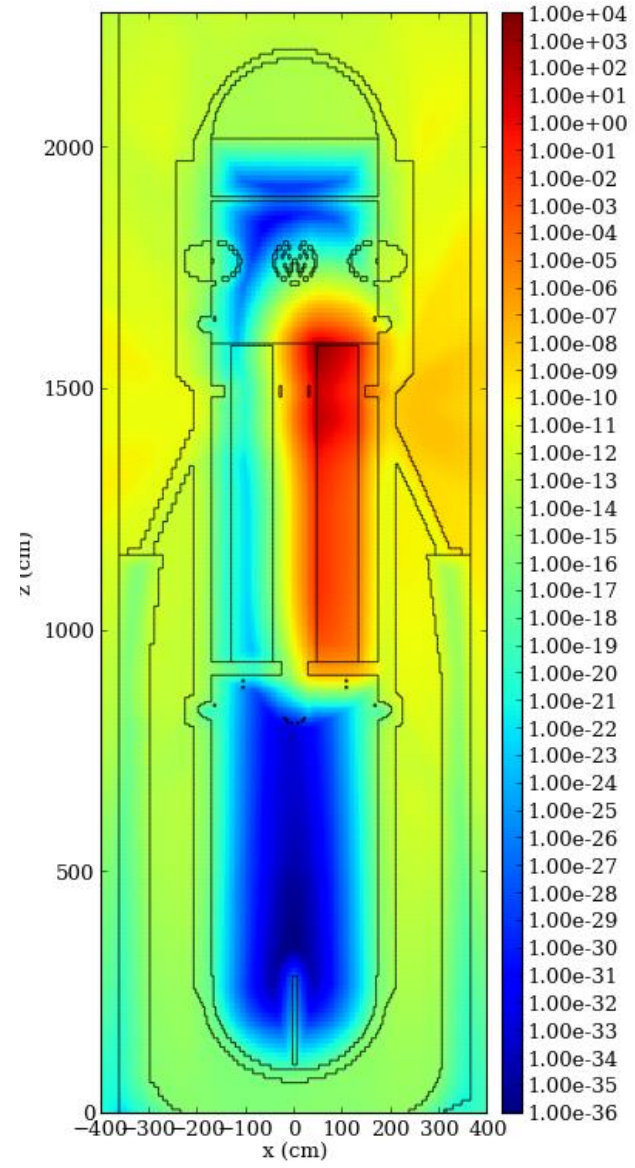


(a) top

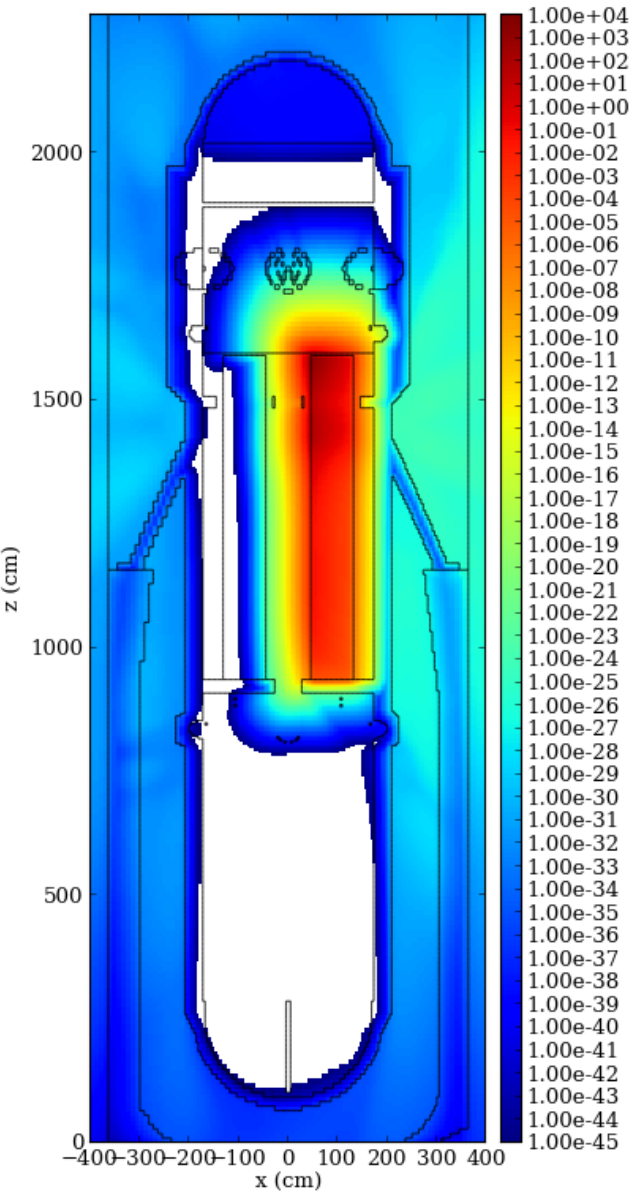
(b) front



group 1

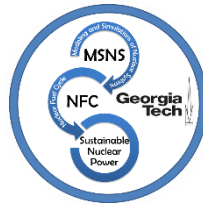


group 100

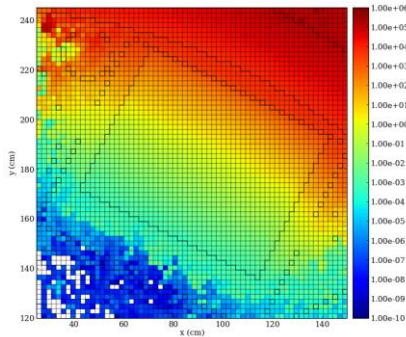


group 238

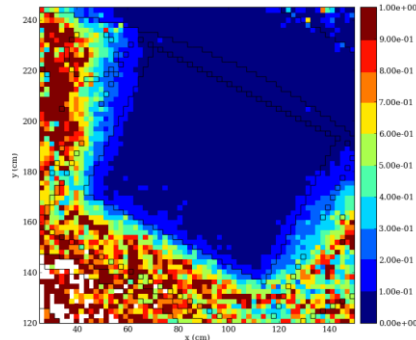
MCHX Activation



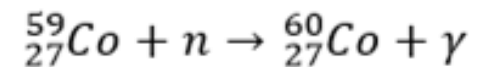
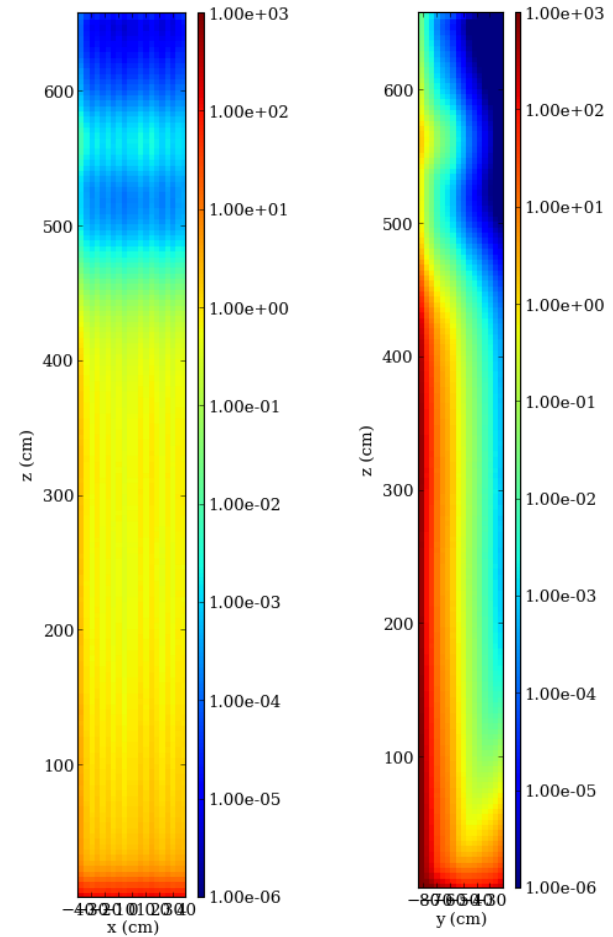
- Biased MC Results
 - 14 parallel runs
 - 4 day wall-clock time (55 day CPU time)
 - 1.3 billion source particles



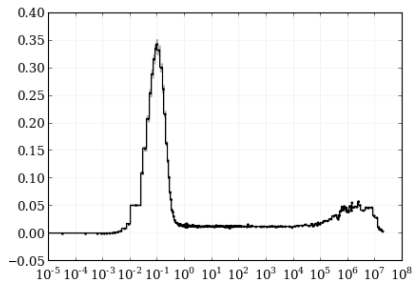
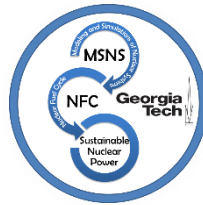
total neutron flux



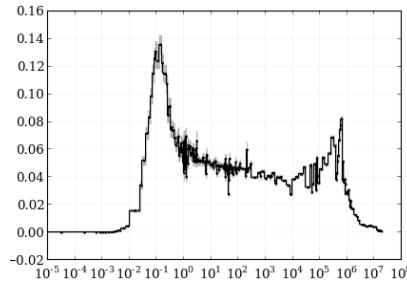
relative uncertainty



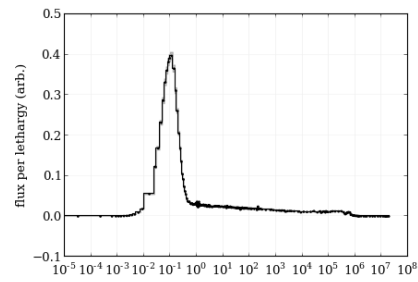
MCHX Activation



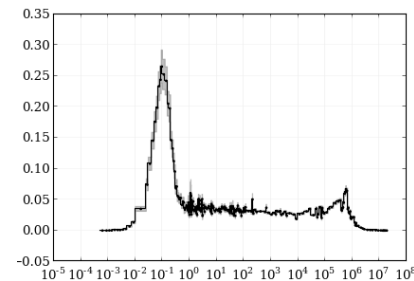
(a) inner side closest to core
 $\sigma_{\square} = 15.5 \pm 0.70\% b$



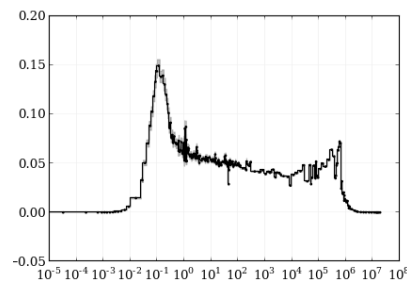
(b) center
 $\sigma_{\square} = 7.35 \pm 1.2\% b$



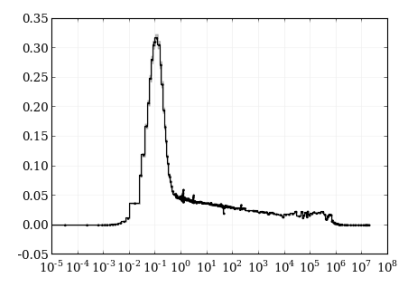
(c) outer edge closest to RPV
 $\sigma_{\square} = 17.8 \pm 0.66\% b$



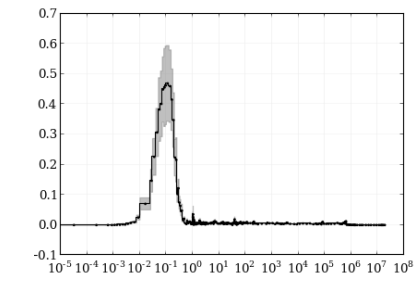
(a) inner side closest to core
 $\sigma_{\square} = 12.2 \pm 2.4\% b$



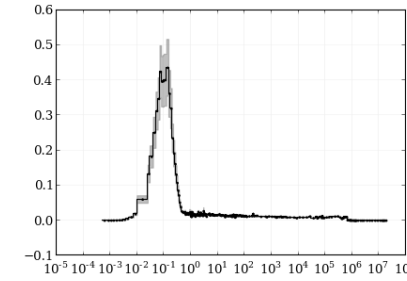
(b) center
 $\sigma_{\square} = 7.64 \pm 1.0\% b$



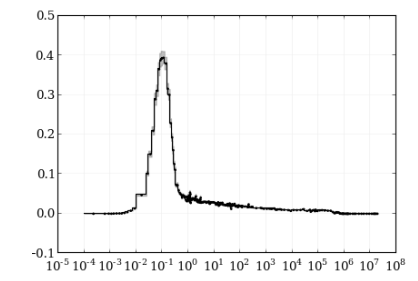
(c) outer edge closest to RPV
 $\sigma_{\square} = 14.2 \pm 0.56\% b$



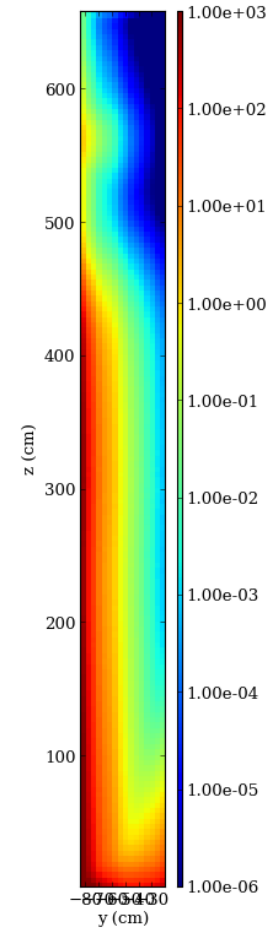
(a) inner side closest to core
 $\sigma_{\square} = 21.6 \pm 7.3\% b$



(b) center
 $\sigma_{\square} = 19.1 \pm 4.7\% b$



(c) outer edge closest to RPV
 $\sigma_{\square} = 17.2 \pm 1.3\% b$

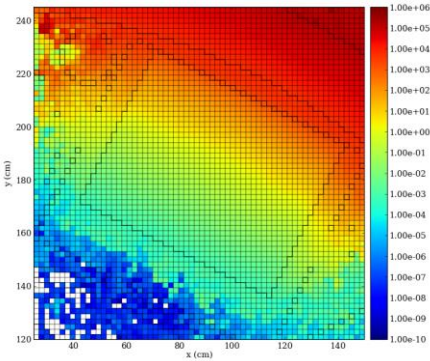


MCHX Activation

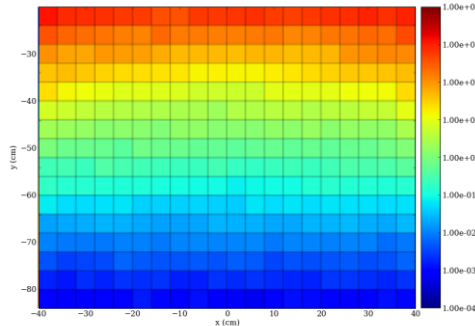
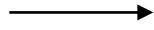
- ORIGEN-S template file
 1. csas-mg (same)
 2. ajax (same)
 3. nitawl (same)
 4. couple (neutron spectra)
 5. origen (total fluence rate)
- Run these in parallel (x32)
- 3.75 hours

```
=csas-mg   parm=(nitawl,chk)
cross sections for couple sample problem
238group
read comp
wtptapmt 1 7.25 7
24000 21
13027 5
42000 3
6000 0.08
14000 0.7
25055 0.4
26000 69.82
0.7 555 end
h2o      1 den=0.765 0.3 555 end
end comp
end
=ajax
0$$ 88 e 1$$ 1 1t
2$$ 11 0 2t
end
=nitawl
0$$ 88 e 1$$ 0 9 e
t
2$$ 24000 13027 42000 6000 14000 25055 26000 8016 1001
t
end
=couple
0$$ a3 80 a5 4 a6 33 e
1$$ a4 1 a15 0 a16 8 0 238 e t
'mchx spectrum
g**
@flux
done
end
=origen
-1$$ 1000000
0$$ a4 33 e
1$$ 1 1t
mchx activation
3$$ 33 a3 1 0 a10 0 a11 0 a12 0 a16 2 a33 47 e t
35$$ 0 4t
56$$ 10 a3 1 0 a13 25 5 3 32 2 1 e
57** a3 1-15 e 5t
mchx activation
mavric fluence rate
@power
60** 0.001 0.01 0.1 5i1 100
65$$ 0 0 0 a4 9r1 a7 9r1 f0 e
66$$ 2 a5 1 a9 1 e
@isotopes
@densities
75$$ 25r4
81$$ 2 0 26 1 a7 200 e
82$$ f2 e
83**
```

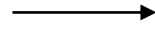

MCHX Activation



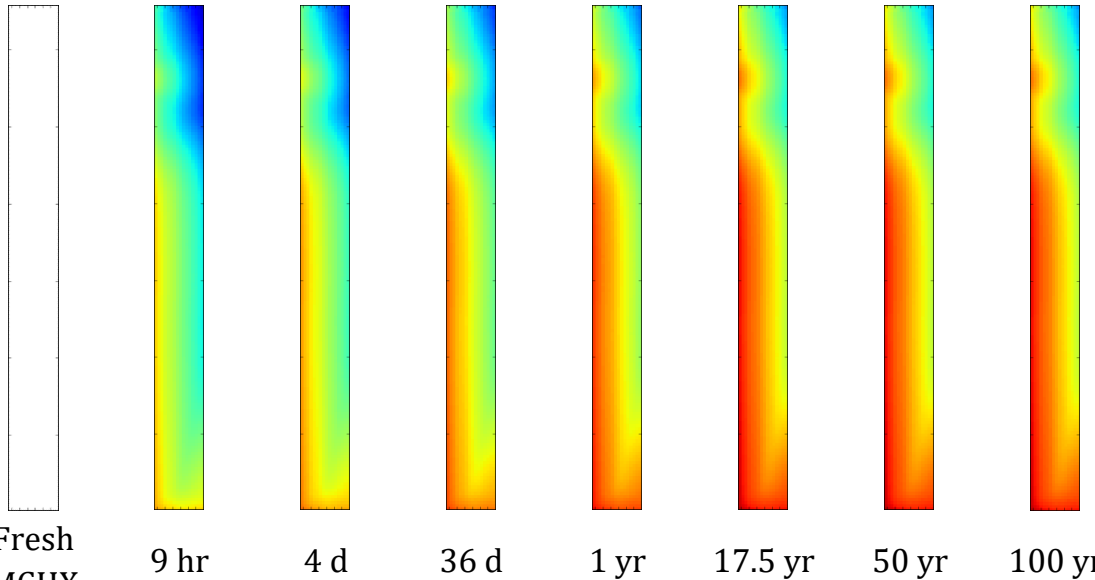
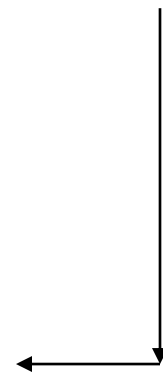
MC results



rotate to normal of MCHX



deplete each voxel w/ ORIGEN-S

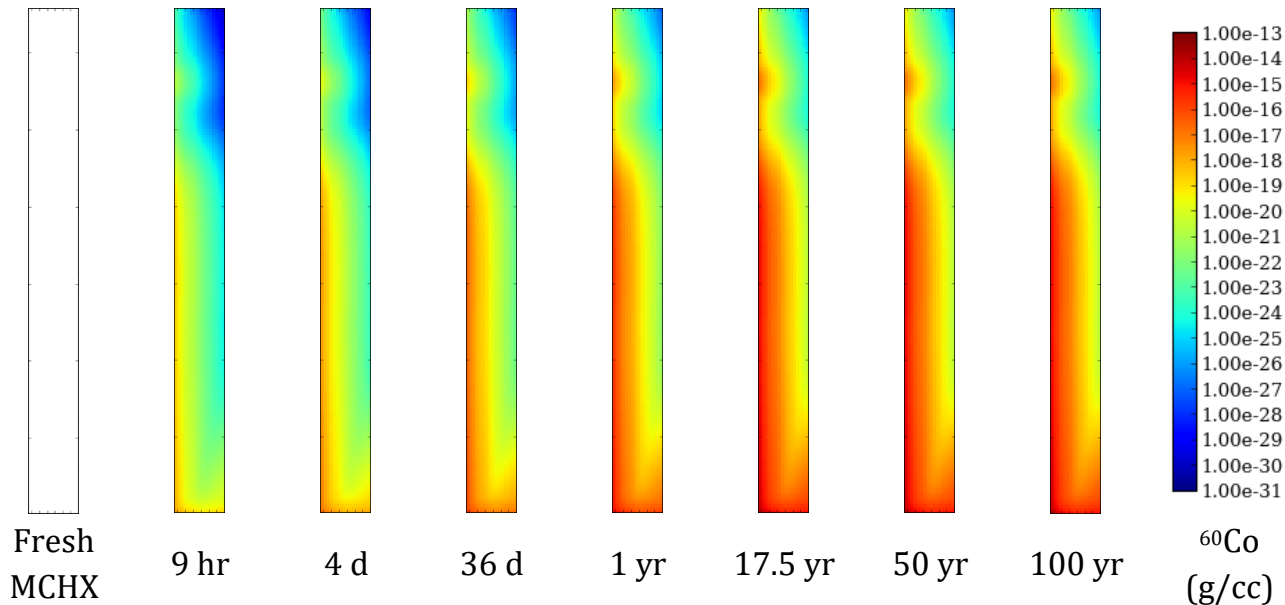


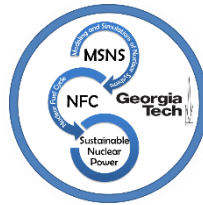
^{60}Co (g/cc)

project time-dependent isotopics, gamma source, etc. to 3Dmap

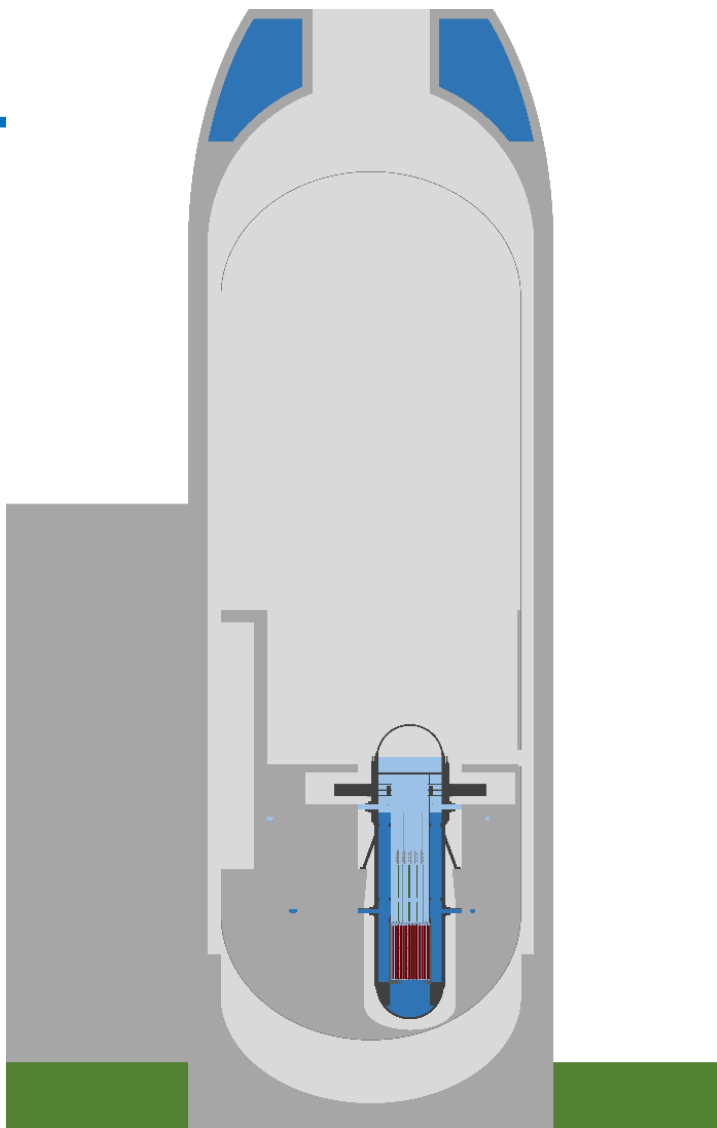
- **CONCLUSION:**

- Max Co-60 at equilibrium (30 years) below IAEA free-release limit
 - » (0.4Bq/g > 0.3 Bq/g)
- Therefore, safe for maintenance with no extra shielding
- May need to cool down for one half-life after decommissioning

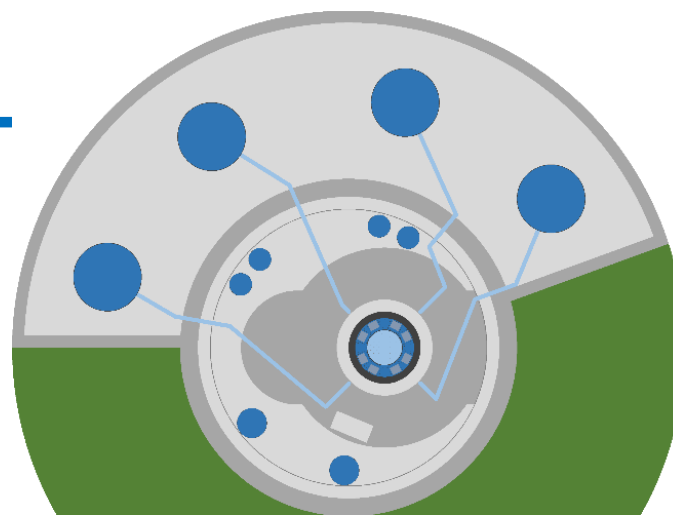




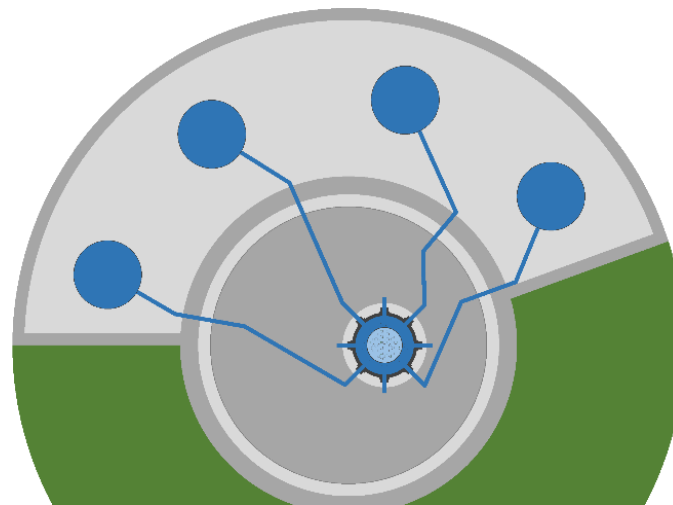
DOSE DISTRIBUTION THROUGHOUT NUCLEAR ISLAND



(a) front view of the shield building enclosing the CV



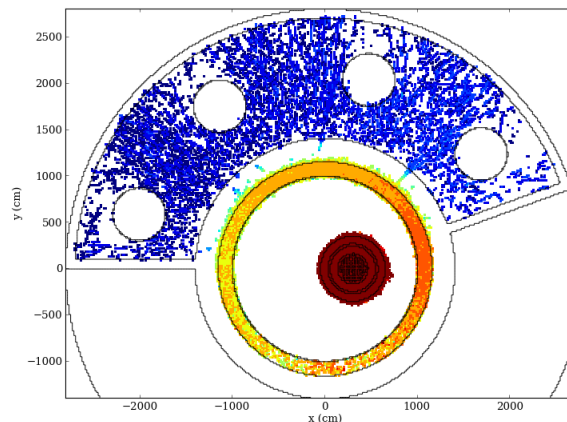
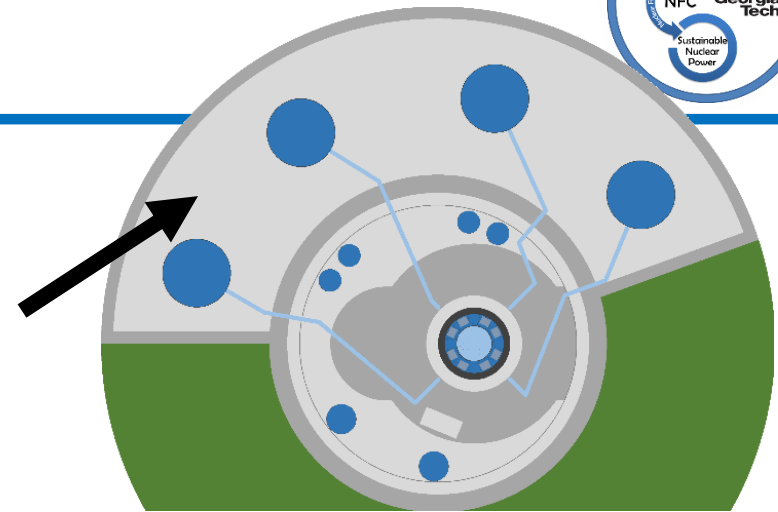
(b) top view showing the hot leg piping from MCHXs to the SGS



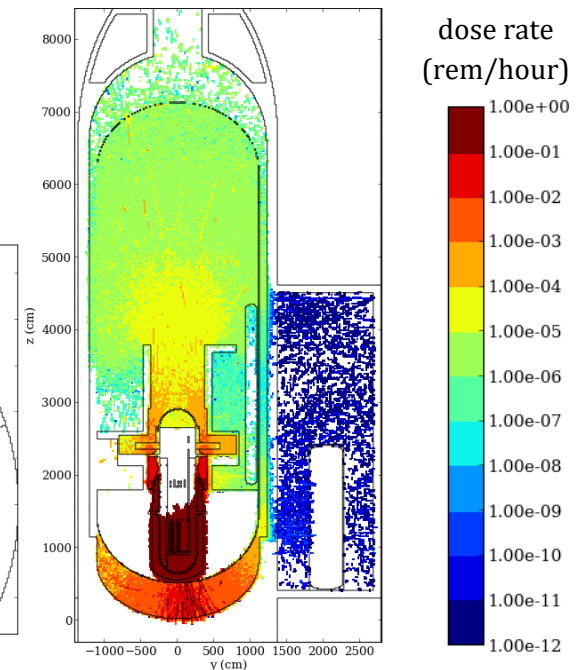
(c) top view showing the cold leg piping from the SGS back to the MCHXs

Dose rate distributions

- Preliminary results
- Adjoint solution
 - adjoint source: n+ γ dose rate in room with flashing drum
 - 46 group library
 - P_1/S_4
 - 320x240x498 mesh
 - » 17 cm side length of voxels
 - 26 hours for forward and adjoint on 32 CPUs
 - ~256Gb of memory
- MC results
 - 1 billion particles
 - 10 runs in parallel



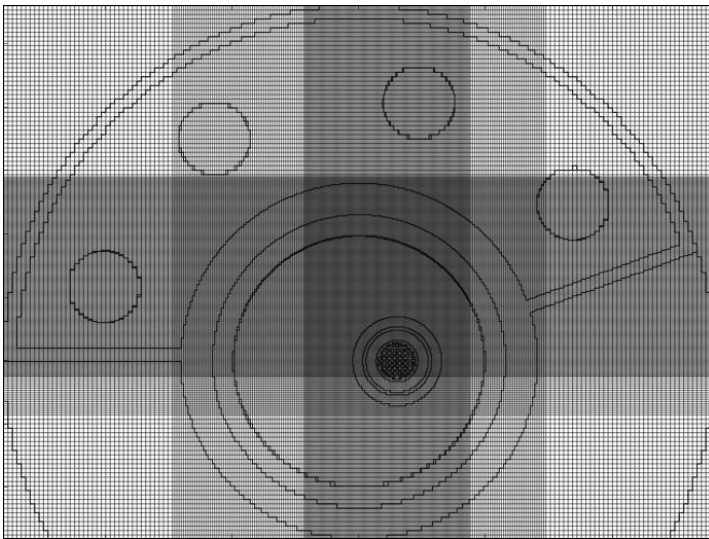
(a) top view



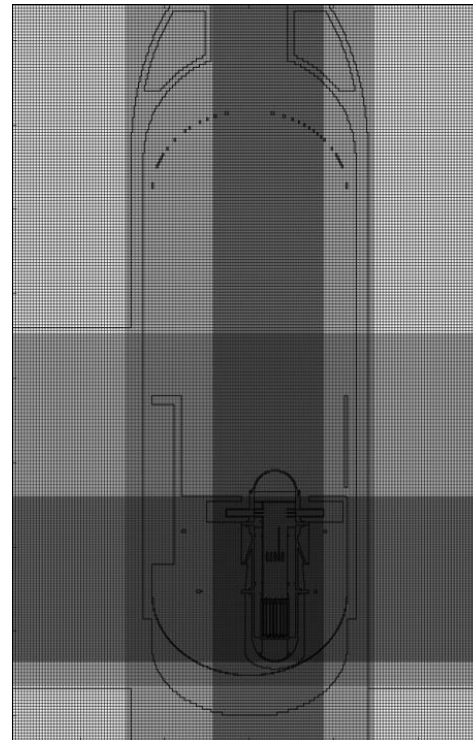
(b) side view

Dose rate distribution

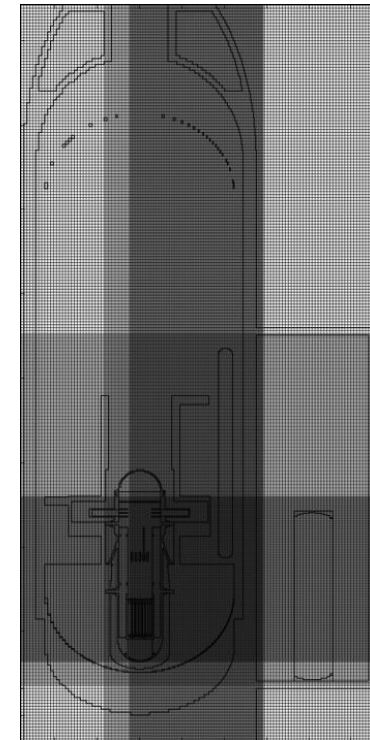
- Good results using mesh refinement
- Adjoint solution
 - 46 group library P_1/S_4 322x267x483mesh (14GB)
 - » 9 cm side length of voxels
 - 32 hours for forward and adjoint on 32 CPUs



(a) top



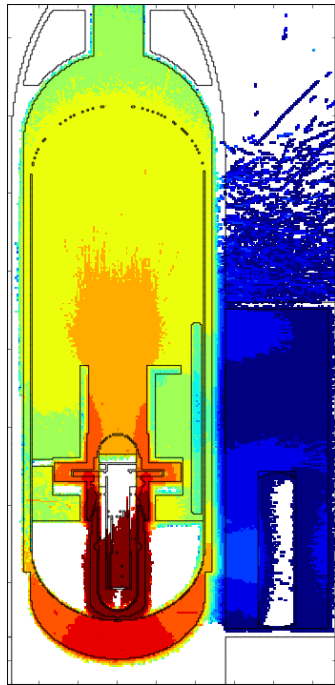
(b) front



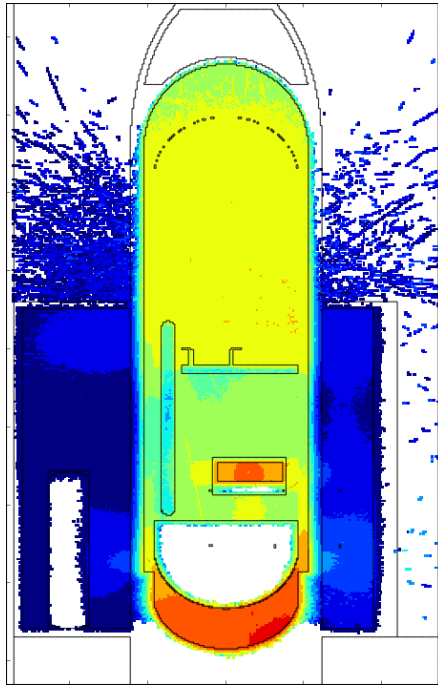
(b) side

VG 35

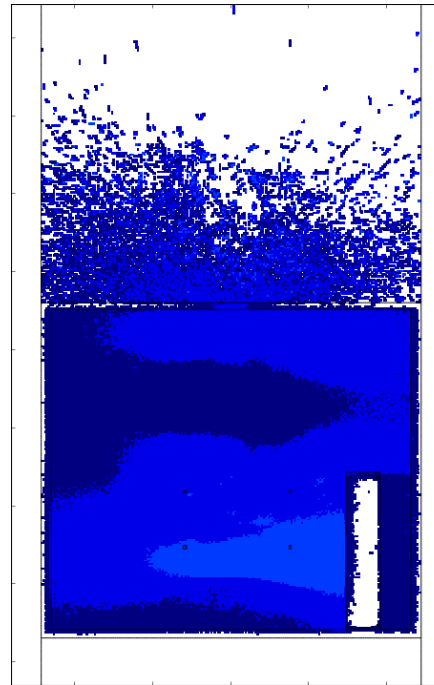
Dose rate distribution



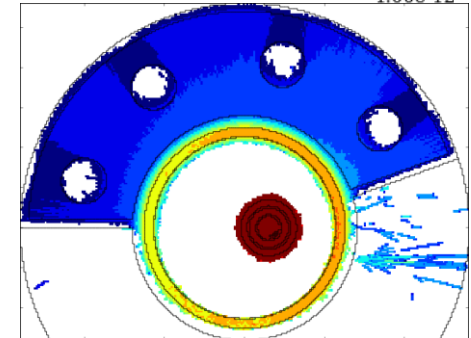
(a) side view
at core
centerline
($x \approx 300 \text{ cm}$)



(b) front view
showing max flux
leaving concrete
shield
($y \approx 800 \text{ cm}$)

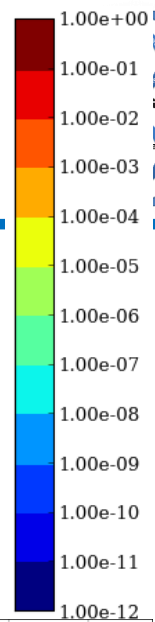


(c) front view
showing large cross
section of SGS room
($y \approx 1450 \text{ cm}$)

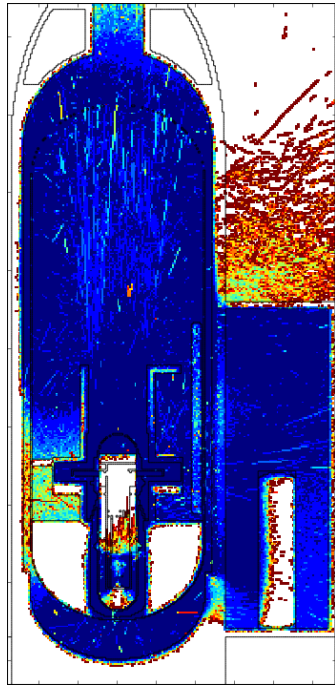
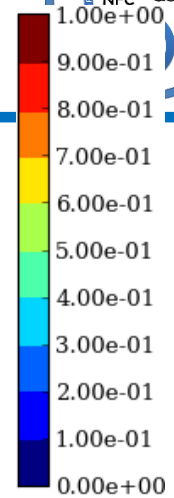


(d) top view at core
centerline and
showing the max flux
leaving concrete
shield
($z \approx 1175 \text{ cm}$)

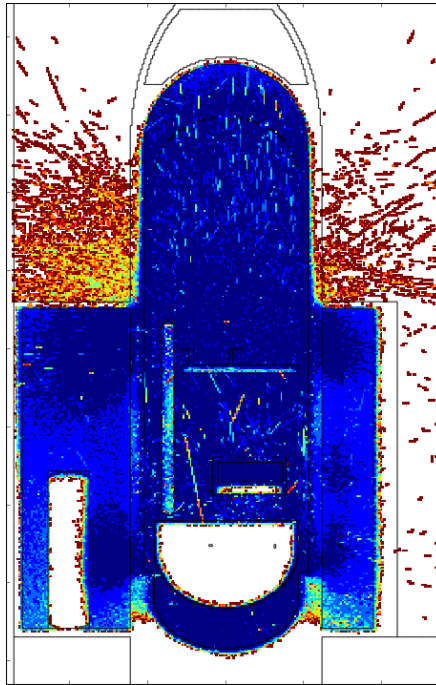
dose rate
(rem/hour)



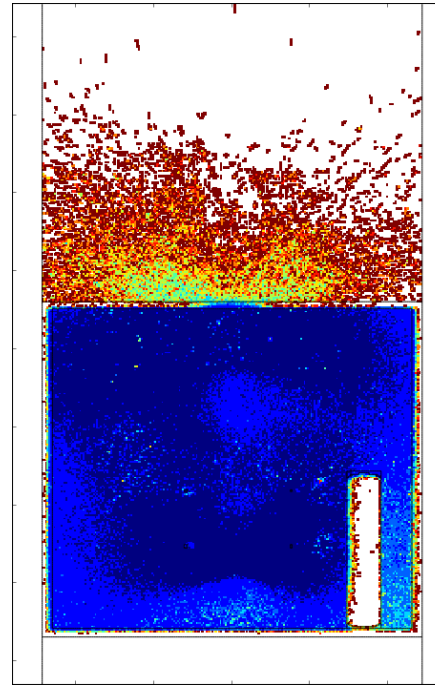
Dose rate distribution



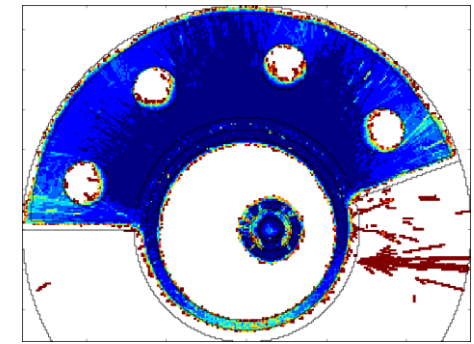
(a) side view
at core
centerline
($x \sim 300\text{cm}$)



(b) front view
showing max flux
leaving concrete
shield
($y \sim 800\text{cm}$)

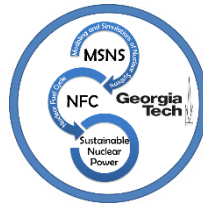


(c) front view
showing large cross
section of SGS room
($y \sim 1450\text{cm}$)

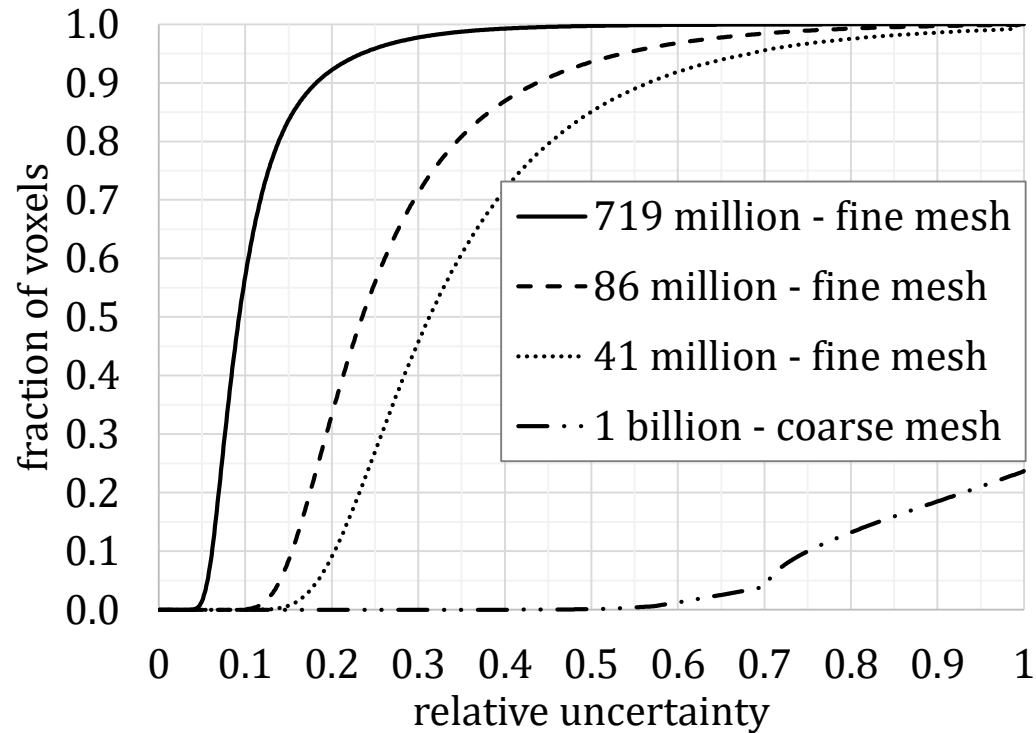


(d) top view at core centerline
and showing the max flux
leaving concrete shield
($z \sim 1175\text{cm}$)

Dose rate distribution

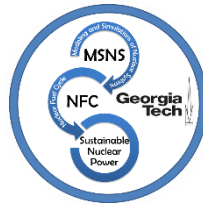


- MC results
 - 10 “parallel” CPUs
 - 719 million source particles
 - 56% of voxels <10% rel. unc.
 - 92% of voxels < 20% rel. unc.
 - 99% of voxels < 35%



- Conclusions
 - Large dose rate problem on detailed model
 - Achieved good results using manually refined mesh

Conclusions



- Demonstrated the use of Scale sequences (MAVRIC, ORIGEN-S COUPLE, KENO) for shielding studies within a large detailed model
- RPV lifetime assessment
- SiC detector Placement
- Gamma heating in radial neutron steel reflector
- MCHX activation
- Dose in nuclear island

