

## Tutorial: Using ORIGAMI for Detailed Spent Fuel Assembly Analysis in Safeguards Applications

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## Outline

- Background of spent fuel safeguards
- Introduction to ORIGEN and <u>ORIG</u>en <u>Asse</u>Mbly <u>I</u>sotopics (ORIGAMI)
- ORIGAMI: descriptions and features
- ORIGAMI tutorial problems



## Spent fuel Safeguards



Spent fuel storage pool [1]

Partial defect tests are required before spent fuel assemblies being transferred to "difficult-to-access" storage.

[1]: <u>https://www.linkedin.com/pulse/performance-improvement-case-study-1-outage-duration-todd-mccann</u>
 [2]: <u>https://www.nrc.gov/reading-rm/doc-collections/fact-sheets/dry-cask-storage.html</u>

[3] https://www.researchgate.net/publication/260877239 The Use of Clay as an Engineered Barr ier in Radioactive-Waste Management - A Review/figures?lo=1





Encapsulation and final disposal [3]

# Overview of ORIGEN

- <u>Oak Ridge Isotope Gen</u>eration code in SCALE
- Irradiation and decay simulation code
- Explicit simulation of nuclides in database
  - 176 actinides
  - 1151 fission products
  - 910 structural activation nuclides
- Explicit simulation of all pathways from neutron transmutation, fission, and decay
  - ORIGEN tracks 2237 isotopes
  - Includes all nuclides with half-lives > 1 ms
  - Accurately represents the evaluated nuclear data
  - Many physics codes track a small subset of isotopes

OAK RIDGE

# Key Capabilities of ORIGEN

- Spent nuclear fuel characterization
  - Nuclide concentrations (atoms and mass)
  - Activities
  - Decay heat
  - Radiation emission rates and spectra (neutron and gamma)
  - Radiotoxicity
- Source terms for accident analyses (operating reactors, spent fuel handling, storage, etc.)
- Structural material activation (in-core, ex-core)
- Fuel cycle analysis (e.g., material feed and removal processing)
- ORIGEN data enable comprehensive isotopic characterization of fuel over a large time scale, including repository analysis

## ORIGAMI: an automated ORIGEN interface for 3D fuel assembly burnup calculation

- A customized user interface of ORIGEN for 3-D assembly burnup calculations.
- Pre-generated cross-section libraries are interpolated to produce accuracies similar to full SCALE/TRITON depletion simulations.
- Can generate nuclide compositions and decay heat for each axial node of each fuel pin based on specified burnup values.
- Accepts different compositions, enrichments, burnup, cross-section libraries for each fuel rod.





# **ORIGAMI** Capabilities

- Enable 3D ORIGEN calculations on a spent fuel assembly
- Input capabilities
  - Account for assembly radial and axial burnup distributions
  - Account for axial moderator density variations
  - Can assign different initial fuel composition (e.g., enrichment, Gd) and ORIGEN library for each pin
  - Assign different power levels on each pin segment
  - Convenient Fulcrum interface
- Output capabilities
  - Complete f71 file and SCALE StdComp mix file
  - Material cards and neutron/gamma source terms for each pin segment, which can be directly used for MCNP and KENO transport models
  - Decay heat for each axial segment of the assembly

Why is high-fidelity spent fuel modeling and simulation needed?

- Detailed nuclide compositions and spatial distribution are needed for 3D NDA modeling and • simulation, in order to quantify instrument performance.
- Calculations provide a) correlations between measured data and the quantities of interest not • directly measured and b) verification of measurements since the actual assembly inventories cannot be measured.



Pin-by-pin burnup map of a 14x14 spent fuel assembly [1]

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[1] J. Hu, I. C. Gauld, J. Banfield and S. Skutnik, "Developing Spent Fuel Assembly Standards for Advanced NDA Instrument Calibration - NGSI Spent Fuel Project," ORNL/TM-2013/576, Oak Ridge National Laboratory, 2014.

[2]: http://modernsurvivalblog.com/nuclear/spent-nuclear-fuel-pools-are-full/

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## **ORIGAMI** results: radial Pu distribution

28.2	27.8	27.5	27.3	27.1	27.0	26.9	25.4	25.3	25.0	24.6	24.0	23.2	22.3
29.6	29.5	29.7	29.1	28.8	29.2	28.7	27.1	27.4	26.8	28.3	26.0	24.8	23.6
31.0	31.4		31.3	31.1		30.7	29.0		28.8	28.3		26.5	24.8
32.1	32.2	32.8	32.5	32.8	32.5	31.5	29.6	30.3	30.2	29.3	28.7	27.2	25.8
33.2	33.4	34.0	34.2		33.4	32.4	30.1	30.9		30.7	29.7	28.1	26.7
34.3	34.9		35.0	34.5	34.0	34.0	30.9	30.9	31.3	31.2		28.2	27.4
35.1	35.2	35.7	34.9	34.4	34.9		31.8	31.0	30.9	30.9	30.7	29.3	27.9
36.2	36.3	36.8	35.9	35.2	34.9	35.0	34.4	33.8	33.6	33.5	33.3	31.7	30.3
37.0	37.7		37.8	37.0	35.8	35.0	34.7	34.8	35.2	35.1		32.8	30.9
37.7	38.0	38.7	38.8		37.3	35.9	35.5	38.3		36.0	34.8	32.9	31.4
38.5	38.7	39.4	39.0	39.2	38.6	37.2	36.8	37.6	37.3	36.2	35.4	33.6	32.1
39.2	39.9		39.8	39.5		38.6	38.2		37.7	37.0		34.8	32.9
39.7	39.8	40.2	39.4	39.1	39.3	38.4	38.2	38.5	37.5	36.9	36.6	35.0	33.6
40.3	40.0	39.7	39.4	39.1	38.8	38.5	38.6	38.3	37.8	37.2	36.5	35.5	34.6



### Pu content (g/MTU) in each Pin [1]

Operator-provided pin-by-pin burnup (GWd/tU) map [1]

[1] J. Hu, I. C. Gauld, J. Banfield and S. Skutnik, "Developing Spent Fuel Assembly Standards for Advanced NDA Instrument Calibration – NGSI Spent Fuel Project," ORNL/TM-2013/576, Oak Ridge National Laboratory, 2014.



## ORIGAMI results: radial Cs-137 distribution

0.86	0.86	0.86	0.87	0.87	0.88	0.88	0.87	0.87	0.87	0.87	0.87	0.87	0.87	0.87
0.86	0.87	0.9	0.88	0.89	0.91	0.89	0.88	0.89	0.91	0.89	0.89	0.91	0.88	0.88
0.87	0.9		0.92	0.93		0.94	0.93	0.94		0.94	0.93		0.92	0.89
0.87	0.89	0.93	0.93	0.95	0.96	0.95		0.96	0.96	0.96	0.94	0.94	0.91	0.9
0.88	0.9	0.93	0.96		0.95	0.92	0.94	0.93	0.96		0.97	0.96	0.92	0.91
0.89	0.92		0.96	0.95	0.92	0.9	0.91	0.91	0.93	0.96	0.98		0.95	0.92
0.89	0.9	0.95	0.96	0.93	0.91	0.91	0.94	0.93	0.92	0.94	0.98	0.98	0.93	0.92
0.89	0.9	0.94		0.94	0.91	0.93		0.94	0.92	0.96		0.97	0.93	0.92
0.89	0.9	0.95	0.96	0.93	0.91	0.92	0.94	0.93	0.92	0.95	0.99	0.98	0.94	0.93
0.89	0.93		0.97	0.96	0.93	0.92	0.92	0.93	0.95	0.98	0.99		0.96	0.94
0.89	0.91	0.95	0.97		0.97	0.95	0.96	0.95	0.98		1	0.98	0.95	0.94
0.9	0.91	0.95	0.96	0.98	0.99	0.98		0.99	1	1	0.98	0.98	0.95	0.94
0.9	0.93		0.96	0.97		0.98	0.98	0.99		0.99	0.98		0.97	0.94
0.9	0.91	0.94	0.93	0.94	0.96	0.94	0.94	0.95	0.97	0.95	0.95	0.97	0.94	0.94
0.91	0.91	0.91	0.92	0.93	0.93	0.93	0.93	0.94	0.94	0.94	0.94	0.94	0.94	0.95

(a) Given burnup distribution (input) [1]



(b) Calculated Cs-137 distribution (output) [1]

[1] J. Hu, et al., "Spent Fuel Modeling and Simulation using ORIGAMI for Advanced NDA Instrument Testing," in ANS M&C 2015, Nashville, TN, 2015.





# ORIGAMI Problem 1: Express form using Fulcrum [1]: A point model

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[1] W. Wieselquist, H. Liljenfeldt, ORIGAMI Spent Fuel Characterization, Scale Users' Group Workshop, ORNL, 2017

# Problem 1: a point model using Fulcrum express form

- Use Fulcrum express form to build a single-point model
- One fuel composition: 4.5% UO2
- One radial and one axial node
- Three uniform cycles with constant irradiation power
- 5 year final cooling time.



# **ORIGAMI** "Express Form"

SCALE	
ïle Edit View Run Help	
eload origami.inp Save origami.inp Save origami.inp	as Close tab Print Cut Copy Paste Undo Redo Find
avigation 🗗 🗙	origami.inp 🔀
Filter	▼ SCALE 6.2 ▼ Run ▼
origami.inp	<pre>1 Csas5 - Criticality safety analysis using KENO V.a csas6 - Criticality safety analysis using KENO V.a csas6 - Criticality safety analysis using KENO-VI csas5 - Criticality safety search using KENO V.a starbucs - Automated criticality safety analyses using burnup credit sourcerer - 3D criticality safety analysis with hybrid starting source generation devc - 3D discrete ordinates eigenvalue analysis with Denovo kmart5 - KENO V.a multigroup post processor for fluxes and reaction rates kenova - Monte Carlo eigenvalue neutron transport module with simplified geometry kenovi - Monte Carlo eigenvalue neutron transport module with generalized geometry t-xsc - Problem-dependent multigroup cross section processing with material aliasing t-capl-1d - 1D discrete ordinates transport sequence t-depl - 2D discrete ordinates transport sequence t-depl - 2D discrete ordinates depletion newt - 2D discrete ordinates depletion newt - 2D discrete ordinates depletion is - D light water reactor depletion with simplified t5-depl - Monte Carlo depletion using KENO V.a t6-depl - Monte Carlo depletion using KENO-VI mavric - Shielding analysis with Monaco using automated variance reduction monaco - Monte Carlo fixed-source neutron and gamma transport origemi - Depletion, decay, and activation analysis tsunami-3d-K5 - 3D sensitivity/uncertainty analysis using KENO V.a tsunami-id - 1D sensitivity/uncertainty analysis using KENO V.a tsunami-id - 3D sensitivity/uncertainty analysis tsunami-3d-K5 - 3D sensitivity/uncertainty analysis tsunami-ip - TSUNAMI indices and parameters for validation sampler - Stochastic uncertainty analysis using KENO-VI tasr - Reactivity sensitivity analysis tsunami-ip - TSUNAMI indices and parameters for alidation sampler - Stochastic uncertainty analysis for any SCALE sequence sams - TSUNAMI sensitivity analysis module tsprece - Problem-dependent multigroup cross section processing mcdancoff - Monte Carlo Dancoff factor calculation using KENO-VI shell - Module to access operating system commands </pre>

- create empty file (origami.inp)
- CTRL+SPACE inside empty file
- choose "origami UO2 express form (configurable)



Balle Fulcrum	8	×				
Parameters						
Origami						
Title	this-is-my-title 🔹					
Fuel Type	w17x17					
Uranium (MTU)	1.0 🗸					
Enrichment (Wt	\$U235) 4.5 ·					
Burnup (MWd/MT	U) 40000 🗸					
Cycles	3					
Number of Burn	up Interpolations per Cycle 4					
Cooling Time (	days) 1825 🔹					
Power History	Power History - Percent Up 95					
Power History	Power History - Average Power (MW/MTU) 40 🗸					
Moderator Dens	Moderator Density (g/cc) 0.7332 -					
	Create Create as new file Para	meter set				
	Template engine results Template engine log Template eng	jine view				
	ОК	Cancel				
		-				

- window will appear
- click "Create"
- click "OK"



# Controlling Cross Section Interpolation (libraries per cycle)







- This is a valid ORIGAMI input!
- click Run



Wed Feb 17 17:13:11 2016 🗵 Wed Feb 17 17:19:44 2016 🔀						
9 *	*					
10 * Reactor and Nuclear Systems Division	*					
11 * Oak Ridge National Laboratory	*					
12 *	*					
13 * http://scale.ornl.gov	*					
14 * scalehelp@ornl.gov	+					
15 *	+					
16	*******					
17 ************************************	*********					
18						
19 Job Information						
20						
21 Job started on PC0091974 on Wed 17/02/2016 17:19:44						
22 Working directory: C:\Users\ww5\AppData\Local\Temp\scale.ww5	.13016					
23 Input file name : C:\Users\ww5\Desktop\origami.inp	23 Input file name : C:\Users\ww5\Desktop\origami.inp					
24 Output file name : C:\Users\ww5\Desktop\origami.out						
SCALE executable : C:\SCALE-6.2/bin/scale						
26						
27 ************************************	*********					
28						
29						
30 Now depleting axial zone: 001, pin: 01-01						
31						
32						
33 Scale job C:/Users/ww5/Desktop/origami.inp is finished.						
34 Output is stored in C:\Users\ww5\Desktop\origami.out						
35						
36 Process finished with 0 return code; ran in 13 secs, finished at W	ed Feb 17 17:19:57 2016					

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ORIGAMI takes a little while...

- performs by default 10 substeps
  - depletion equal length
  - decay rule of 3s
- nlib=4 would require 4 cases in ORIGEN
- the input has (4+4+4)\*10=120 depletion solves and (1+1+0+1)\*10=30 decay solves.

stale SCALE	
File Edit Vie	ew Run Help
Reload origami.in	Save origami.inp Save origami.inp as Close origami.inp Print   Cut Copy Paste   Undo
Navigation	🗗 🗙 origami.inp 🔀
Filter	document ▼ SCALE 6.2 ▼ Run ▼
▲ origami.inp	1=origami
▷ docum	Reload 2
	Close 4 options{ mtu=1.0 ft71=all}
	Open associated files  origami.assm.f71 ·7x17"]
	origami.f71 ) { enrich=4.5 }
	origami.msg comps=[ fuel=100
	origami.out
	modz = [0.7332]
	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	<pre>13 cycle{ power=40 burn=333. 14 cycle{ power=40 burn=323</pre>

- ORIGAMI produces
   .f71 and .assm.f71
   by default
- open .f71
  - right-click on origami.inp in navigation pane
  - open associated files
  - origami.f71



# **ORIGAMI** Problem 2:

# An example of safeguards application:

A 3 x 3 lattice model

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# Problem 2: A 3 x 3 lattice model

- 3 x 3 lattice with a guide tube
- Two different fuel compositions
- Radial power (burnup) profile
- Three axial nodes with axial power profile
- Three non-uniform cycles
- Request neutron/gamma emission spectra after 5-year cooling time





## ORIGAMI Output Files

### \*\_AxialDecayHeat

2.78253E+02 5.89804E+02 2.17135E+02

#### \*\_ MCNP\_matls.inp

C Axial zon	e: 03,	Pin: 008
C Zone mass	(grams	): 2.144858E+04
m803 1001	-8.5	98225E-09
	1002	-6.035635E-10
	1003	-2.526046E-08
	2003	-8.794443E-09
	2004	-3.262135E-06
	3006	-2.660487E-17
	3007	-7.905803E-18
	4009	-5.885097E-13
	5010	-6.966128E-17
	5011	-4.479028E-15

#### \*\_ MCNP\_neutron.inp

C Neutron source for axial zone 03, pin 001 C Total intensity (n/sec): 5.2826E+05 SI103 H 2.5000E-08 1.0000E-01 1.0000E+00 2.0000E+01 SP103 D 1.1249E-02 2.5571E-01 7.3304E-01

#### Much more info in the main output file "\*.out"

Nuclide concentrations in grams, actinides for case 'axial zone: 001, pin: 03-01' (#6) multi-pin; multi-library = (relative cutoff; integral of concentrations over time > 1.00E-04 % of integral of all 1290.000d 1290.093d 1290.278d 1290.834d 1292.503d 1297.510d 131 1.8117E+00 1.8117E+00 1.8118E+00 1.8122E+00 u-234 1.8117E+00 1.8119E+00 1.81 u-235 6.6208E+01 6.6208E+01 6.6208E+01 6.6208E+01 6.6208E+01 6.6209E+01 6.62 u-236 5.0132E+01 5.0132E+01 5.0132E+01 5.0132E+01 5.0133E+01 5.0133E+01 5.01 1.7853E+04 1.7853E+04 u-238 1.7853E+04 1.7853E+04 1.7853E+04 1.7853E+04 1.78 np-237 6.2240E+00 6.2248E+00 6.2263E+00 6.2307E+00 6.2425E+00 6.2679E+00 6.29 pu-238 2.7486E+00 2.7491E+00 2.7500E+00 2.7527E+00 2.7589E+00 2.7694E+00 2.78 pu-239 9.3958E+01 9.3987E+01 9.4044E+01 9.4197E+01 9.4530E+01 9.4935E+01 9.50 pu-240 4.6659E+01 4.6659E+01 4.6659E+01 4.6659E+01 4.6659E+01 4.6659E+01 4.66 pu-241 2.4857E+01 2.4856E+01 2.4856E+01 2.4854E+01 2.4848E+01 2.4832E+01 2.47 pu-242 1.2514E+01 1.2514E+01 1.2514E+01 1.2514E+01 1.2514E+01 1.2515E+01 1.25 am-241 9.5200E-01 9.5231E-01 9.5292E-01 9.5475E-01 9.6025E-01 9.7675E-01 1.02 am-243 2.3995E+00 2.4002E+00 2.4008E+00 2.4010E+00 2.3990E+00 2.4010E+00 2.40 cm-242 2.9934E-01 2.9937E-01 2.9941E-01 2.9925E-01 2.9771E-01 2.9156E-01 2.73 cm-244 9.0308E-01 9.0315E-01 9.0316E-01 9.0314E-01 9.0301E-01 9.0254E-01 9.01 cm-245 4.8234E-02 4.8234E-02 4.8234E-02 4.8234E-02 4.8234E-02 4.8234E-02 4.82 totals 1.8163E+04 1.8163E+04 1.8163E+04 1.8163E+04 1.8163E+04 1.8163E+04 1.81

## Import ORIGAMI results into MCNP detector models

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sdef cel d10 pos 0 0 0 rad d2 ext d3 axs d4 erg=d101 par=1 si10 l 2001:402:403:601 sp10 1 С si2 0 0.4096 sp2 -21 1 c extent of the source si3 -182.88 182.88 sp3 0 1 c axis of the source si4 1 0 0 1 sp4 1 С c neutron spectrum c total neutron emission: 5.475684E+07 n/s/0.1MTU SI101 Н 1.00E-04 1.00E-03 1.00E-02 3.00E-02 6.00E-02 1.00E-01 2.00E-01 4.00E-01 6.00E-01 8.00E-01 1.00E+00 2.00E+00 3.00E+00 4.00E+00 5.00E+00 6.00E+00 7.00E+00 8.00E+00 9.00E+00 1.00E+01 1.20E+01 1.40E+01 1.60E+01 1.80E+01 2.00E+01 SP101 D 0 6.19E+02 1.95E+04 8.42E+04 1.88E+05 3.30E+05 1.09E+06 2.83E+06 3.29E+06 3.49E+06 3.53E+06 1.58E+07 1.11E+07 6.53E+06 3.35E+06 1.64E+06 8.02E+05 3.81E+05 1.77E+05 8.06E+04 5.20E+04 9.93E+03 1.82E+03 3.21E+02 5.52E+01



## **ORIGAMI** Problem 3:

# Detailed form using Fulcrum:

## A 2 x 2 lattice model

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[1] W. Wieselquist, H. Liljenfeldt, ORIGAMI Spent Fuel Characterization, Scale Users' Group Workshop, ORNL, 2017

# Problem 3: A 2 x 2 lattice model using detailed form

- 2 x 2 lattice
- Two different fuel compositions
- Radial power (burnup) profile
- One long cycle with constant power
- Ten axial nodes with axial power profile
- Nonfuel components



# ORIGAMI input from scratch



- **Libs** reactor library
- **fuelcomp** declare mixtures (single mixture problems use 1)
- **hist** operating history

## This is all that is needed to run ORIGAMI.



#### origami.inp\* 🗵

▼ SCALE 6.2 ▼ Run ▼ View... Edit...

1	
csas5 csas6 csas5s starbucs sourcerer devc kmart5 kmart6 kenova kenovi t-xsec t-xsdrn t-depl-1d newt t-newt	<ul> <li>Criticality safety analysis using KENO V.a</li> <li>Criticality safety analysis using KENO-VI</li> <li>Criticality safety search using KENO V.a</li> <li>Automated criticality safety analyses using burnup credit</li> <li>3D criticality safety analysis with hybrid starting source generation</li> <li>3D discrete ordinates eigenvalue analysis with Denovo</li> <li>KENO V.a multigroup post processor for fluxes and reaction rates</li> <li>KENO-VI multigroup post processor for fluxes and reaction rates</li> <li>Monte Carlo eigenvalue neutron transport module with simplified geometry</li> <li>Monte Carlo eigenvalue neutron transport module with generalized geometry</li> <li>Problem-dependent multigroup cross section processing with material aliasing</li> <li>1D discrete ordinates transport sequence</li> <li>2D discrete ordinates transport module</li> </ul>
t-depl polaris t5-depl t6-depl mavric monaco origen origami	<ul> <li>2D discrete ordinates transport sequence</li> <li>2D discrete ordinates depletion</li> <li>2D light water reactor depletion with simplified</li> <li>Monte Carlo depletion using KENO V.a</li> <li>Monte Carlo depletion using KENO-VI</li> <li>Shielding analysis with Monaco using automated variance reduction</li> <li>Monte Carlo fixed-source neutron and gamma transport</li> <li>Depletion, decay, and activation analysis</li> <li>UO2 express form (configurable)</li> </ul>
origami	- Depletion module for reactor assemblies
opus tsunami-1d tsunami-2d tsunami-3d-k5 tsunami-3d-k6 tsar tsunami-ip tsurfer sampler sams xsproc mcdancoff aboll	<ul> <li>ORIGEN post processing utility</li> <li>1D sensitivity/uncertainty analysis</li> <li>2D sensitivity/uncertainty analysis using KENO V.a</li> <li>3D sensitivity/uncertainty analysis using KENO-VI</li> <li>Reactivity sensitivity analysis</li> <li>TSUNAMI indices and parameters for validation</li> <li>TSUNAMI data assimilation tool for validation</li> <li>Stochastic uncertainty analysis for any SCALE sequence</li> <li>TSUNAMI sensitivity analysis module</li> <li>Problem-dependent multigroup cross section processing</li> <li>Module to account operating seater commande</li> </ul>

• Create new input file

 CTRL + SPACE and select origami (not UO2 express form)



- Put marker inside of origami sequence
- CTRL + SPACE and select libs
- Repeat for fuelcomp



- Put marker inside of fuelcomp sequence
- CTRL + SPACE and select uox
- Repeat for mix

origami.inp\* 🗵 SCALE 6.2 ▼ Run ▼ View... Edit... document 🔻 1=origami 2libs=[ w17x17 ] <sup>3</sup>fuelcomp{ 4uox(fuel){ enrich=5.0 8 9mix(1) { comps[ fuel=100.0 ] } 10 11 % insert fuelcomp components here 12 13 14 hist [ 15 16 cycle 17 % insert cycles here 18 19 20 21 % insert origami components here 22 <sup>23</sup> end **CAK RIDGE** 

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- Put marker outside fuelcomp but inside origami
- CTRL + SPACE and select hist
- Repeat for cycle (inside hist)

#### origami.inp\* 🗵

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document ▼ SCALE 6.2 ▼ Run ▼ View...↓ Edit...↓

```
<sup>1</sup>=origami
 2libs=[ w17x17 ]
 <sup>3</sup>fuelcomp{
 4uox(fuel) {
 5
     enrich=5.0
 6
 8 }
 9mix(1) { comps[ fuel=100.0 ] }
10
    insert fuelcomp components here
11
  응
12
13
<sup>14</sup>hist[
15 cycle { power=40 burn=365 down=31 }
16
17
18 응
    insert cycles here
19
20
21
22
    insert origami components here
  읗
23
<sup>24</sup> end
```

#### Final input should look something like this.

#### Or cleaned up:



# **ORIGAMI** input: Options

0	rigami.inp* 🗵	origami.out 🗵			
do	document ▼ SCALE 6.2 ▼ Run ▼ View↓ Edit↓				
1 2 3 4	<b>=origami</b> title="Or: options{	igami depletion and decay"			
- 5 6 7 8 9 10	<pre>interp stdcomp small decayheat restart relnorm mcnp solver fdens temper mtu fracnf nz nburn ndecay output ft71 offsetz pitch</pre>	<pre>/x17 ] uox(fuel){enrich=5.0} mix(1){ comps[ fuel=100.0 ] } } Le{ power=40 burn=2500 down=3650 }]</pre>			

## miscellaneous input

### • mtu

- metric tons of initial heavy metal (not just U)
- used to convert to power in MW
- DEFAULT: 1 MTU

## • ft71

- flag to write f71 file last/cycle/all
- other options
  - **stdcomp** write SCALE StdComp blocks
  - decayheat write file with axial decay heat



# **ORIGAMI** spatial variation

- power shape  $\rightarrow$  axial & radial  $\rightarrow p(z) \times p(x, y)$
- moderator density  $\rightarrow$  axial only  $\rightarrow$  m(z)
- fuel composition  $\rightarrow$  radial only  $\rightarrow c(x, y)$



 $\begin{array}{c} p(x,y) \times p(z) \\ m(z) \\ c(x,y) \end{array}$ 



# **ORIGAMI** spatial variation

- limitations
  - no time-dependence
  - axially-dependent compositions really needed for BWRs





# ORIGAMI Input: Radial and axial distributions

```
origami.inp* 🗵
                origami.f71 🗵
document ▼ SCALE 6.2 ▼ Run ▼ View... Edit...
 <sup>1</sup>=origami
 <sup>2</sup>title="Origami depletion and decay 2x2 fuel array"
 <sup>3</sup>libs=[ w17x17 w15x15 ]
 4libmap=[ 1 2
 5
              2 1 ]
 6 fuelcomp{
       uox(fuel) {enrich=5.0}
       mix(1) { comps[ fuel=100.0 ] }
       uox(fuel2){enrich=4.0}
       mix(2) { comps[ fuel2=100.0 ] }
10
11 }
12 \text{ compmap} = \begin{bmatrix} 2 & 1 \end{bmatrix}
                12]
13
14 hist[ cycle{ power=20 burn=2500 down=3650 }]
<sup>15</sup> pxy=[ 0.80 1.00
16
          1.00 0.80 ]
<sup>17</sup> pz=[ 0.2 0.5 0.8 1.0 1.1 1.15 1.2 0.9 0.6 0.3 ]
<sup>18</sup> end
```

Axial and radial power distribution

- pxy, pz
  - power shape (unitless)
  - renormalized by default
- All zones same cool time
- All axial nodes same material and reactor libraries



# ORIGAMI Input: modz and meshz

```
origami.inp 🔯
document ▼ SCALE 6.2 ▼ Run ▼ View... Edit...
                                                                               meshz - used to evaluate
 1=origami
                                                                               non-uniform axial nodes.
<sup>2</sup>title="Origami depletion and decay 2x2 fuel array"
3 options{ decayheat=yes stdcomp=yes }
                                                                                - pz +1 number of entries
4libs=[ w17x17 w15x15 ]
<sup>5</sup>libmap=[ 1 2
                                                                            • modz - used to evaluate
 6
            2 1 ]
                                                                               changing moderator density
7fuelcomp{
      uox(fuel) {enrich=5.0}
 8
                                                                                - Same number of entries as pz
      mix(1) { comps[ fuel=100.0 ] }
                                                                                - Requires moderator density
      uox(fuel2){enrich=4.0}
10
11
      mix(2) { comps[ fuel2=100.0 ] }
                                                                                   interpolation in reactor library
12 }
                                                                                   or will always use same
13 \text{ compmap} = \begin{bmatrix} 2 & 1 \end{bmatrix}
                                                                                   value.
14
              121
15 hist[ cycle{ power=20 burn=2500 down=3650 }]
<sup>16</sup> pxy=[ 0.80 1.00
         1.00 0.80 ]
17
18 pz=
          [0.20\ 0.50\ 0.80\ 1.00\ 1.10\ 1.15\ 1.20\ 0.90\ 0.60\ 0.30]
19 \mod z =
          [0.75 \ 0.74 \ 0.73 \ 0.72 \ 0.71 \ 0.70 \ 0.69 \ 0.68 \ 0.67 \ 0.66 ]
^{20} meshz= [ 0 10
                      50
                            100 150 200
                                             250
                                                   300 350
                                                               360
                                                                    370 1
<sup>21</sup> end
```

# **ORIGAMI** Input: Non-fuel components

```
origami.inp 🛛
document ▼ SCALE 6.2 ▼ Run ▼ View... Edit...
 <sup>1</sup>=origami
 <sup>2</sup>title="Origami depletion and decay 2x2 fuel array"
 3options{ decayheat=yes stdcomp=yes }
 4libs=[ w17x17 w15x15 ]
 <sup>5</sup>libmap=[ 1 2
 6
             211
 7fuelcomp{
       uox(fuel) {enrich=5.0}
       mix(1) { comps[ fuel=100.0 ] }
       uox(fuel2) {enrich=4.0}
10
11
       mix(2) { comps[ fuel2=100.0 ] }
12
13 compmap= [ 2 1
14
               121
15 hist[ cycle{ power=20 burn=2500 down=3650 }]
<sup>16</sup> pxy=[ 0.80 1.00
17
          1.00 0.80 ]
18 pz=
           [0.20\ 0.50\ 0.80\ 1.00\ 1.10\ 1.15\ 1.20\ 0.90\ 0.60\ 0.30]
<sup>19</sup> modz= \begin{bmatrix} 0.75 & 0.74 & 0.73 & 0.72 & 0.71 & 0.70 & 0.69 & 0.68 & 0.67 & 0.66 \end{bmatrix}
^{20} meshz= [ 0 10
                        50
                              100 150 200 250 300 350 360 370 ]
<sup>21</sup>nonfuel[ zirc4=200 co=0.02 ]
<sup>22</sup> end
```

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- **nonfuel** is given in kg per MTU
  - Give value pairs of standard compositions (i.e. Zirc4), nuclides (i.e. zr-94) or elements (Zr)
  - Can be used to activate cladding, top and bottom nozzles, spacers, fuel channels, control rods/blades, etc.

# **ORIGAMI** Input: Sources

origami.inp\* 🔀

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```
document ▼ SCALE 6.2 ▼ Run ▼ View... Edit...
 1=origami
<sup>2</sup>title="Origami depletion and decay 2x2 fuel array"
3 options{ decayheat=yes stdcomp=yes }
 4libs=[ w17x17 w15x15 ]
<sup>5</sup>libmap=[ 1 2
            2 1
 7fuelcomp{
      uox(fuel){enrich=5.0}
      mix(1) { comps[ fuel=100.0 ] }
      uox(fuel2) {enrich=4.0}
11
      mix(2) { comps[ fuel2=100.0 ] }
12 }
^{13} compmap=[ 2 1
             12]
15 hist[ cycle{ power=20 burn=2500 down=3650 }]
<sup>16</sup> pxy=[ 0.80 1.00
17
         1.00 0.80 ]
18 pz=
          [ 0.20 0.50 0.80 1.00 1.10 1.15 1.20 0.90 0.60 0.30 ]
19 \mod z = [0.75 \ 0.74 \ 0.73 \ 0.72 \ 0.71 \ 0.70 \ 0.69 \ 0.68 \ 0.67 \ 0.66]
20 meshz= [ 0 10 50 100 150 200 250 300 350 360 370 ]
<sup>21</sup>nonfuel[ zirc4=200 co=0.02 ]
22 srcopt {
23
      sublib=all
24
25
26
27 }
      brem medium=uo2
      alphan medium=case
      print=no
28 gqrp=[ 3.0E+06 2.5E+06 2.0E+06 1.5E+06 1.0E+06 0.7E+06 0.4E+06 ]
<sup>29</sup>ngrp=[ 20.0E+06 6.4E+06 3.0E+06 1.8E+06 1.4E+06 0.9E+06 0.4E+06 0.1E+06 ]
<sup>30</sup> end
```

- **scropt** options for neutron and gamma sources
- **ggrp, ngrp** gamma/neutron group structure
  - Given as boundaries in descending order

# **ORIGAMI** Input: Print

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origami.inp 🛛 document ▼ SCALE 6.2 ▼ Run ▼ View... Edit... 1=origami <sup>2</sup>title="Origami depletion and decay 2x2 fuel array" 3 options{ decayheat=yes stdcomp=yes } 4 libs=[ w17x17 w15x15 ] <sup>5</sup>libmap=[ **1 2 2 1** ] 6 fuelcomp{uox(fuel) { enrich=5.0} mix(1) { comps[ fuel= 100.0 ] } uox(fuel2){enrich=4.0} mix(2) { comps[ fuel2=100.0 ] } } <sup>8</sup> compmap=[ 2 1 1 2 ] 9hist[ cycle{ power=20 burn=2500 down=3650 }] <sup>10</sup> pxy=[ 0.80 1.00 1.00 0.80 ] [ 0.20 0.50 0.80 1.00 1.10 1.15 1.20 0.90 0.60 0.30 ] 11 pz= [ 0.75 0.74 0.73 0.72 0.71 0.70 0.69 0.68 0.67 0.66 ]  $12 \mod z =$ 100 150 200 250 300 350 360 370  $^{13}$ meshz= [ 0 10 50 <sup>14</sup>nonfuel[ zirc4=200 co=0.02 ] <sup>15</sup>srcopt{ sublib=all brem medium=uo2 alphan medium=case print=no} <sup>16</sup>ggrp=[ 3.0E+06 2.5E+06 2.0E+06 1.5E+06 1.0E+06 0.7E+06 0.4E+06 ] <sup>17</sup>ngrp=[ 20.0E+06 6.4E+06 3.0E+06 1.8E+06 1.4E+06 0.9E+06 0.4E+06 0.1E+06 ] 18 print { 19 nuc{ 20 sublibs=[ lt ac fp ] 21 22 23 24 total=yes units=[ grams watts curies ] <sup>25</sup>nuccomp=[ 8016 92234 92235 92236 92238 93237 94238 94239 94240 94241 94242 95241 95243 42095 43099 44101 45103 47109 55133 60143 60145 62147 26 27 62149 62150 62151 62152 63151 63153 64155 ] 28 end

- print sets what is shown in the output for last time step
  - Select between nuclides (nuc) or element (ele)
  - Sublibs, can be light elements (It), actinides (ac), fission products (fp) or all.
  - total = yes will print the total concentration for each output unit type